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REVISION OF
THE
PRELIMINARY PROPOSAL
FOR

UPRATING THE AIR CONDITIONING UNIT,
NEW WING, BIO-MEDICAL BUILDING

CENTER FOR ENERGY AND ENVIRONMENT RESEARCH
RIO PIEDRAS, PUERTO RICO

February, 1979

Prepared by;

SOLAR DIVISION
CENTER FOR ENERGY AND ENVIRONMENT RESEARCH
CAPARRA HEIGHTS STATION
SAN JUAN, PUERTO RICO



CENTER FOR ENERGY AND ENVIRONMENT RESEARCH
UNIVERSITY OF PUERTO RICO — U.S. DEPARTMENT OF ENERGY

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I. Purpose and Source of Funds

The purpose of this revised proposal is to describe the requirements to upgrade the Air Conditioning System in the New Wing of the Bio-medical building, Center for Energy and Environment Research (C.E.E.R.), Río Piedras, Puerto Rico; to define the facilities in engineering terms and establish a reasonable budget cost estimate and time schedule, and to recommend an appropriate method of accomplishment.

Three main items will be addressed with this proposal:

1. Provide a reliable air conditioning system that will meet the needs of the laboratory and office building.
2. Use the thermal waste heat available from a 50,000 ft² Solar Photovoltaic Concentrator Array to be installed at the C.E.E.R. under a nation wide program sponsored by the U. S. Department of Energy.
3. Upgrade the building envelope and building ventilation and air handling systems to be in accordance with the present energy conservation regulations now being implemented in Puerto Rico.

As a final result of this proposal a dramatic reduction in operating cost for the air conditioning system in the New Wing of the C.E.E.R. will be obtained.

We propose that the design and construction for this work will be charged to General Plant Project FY-1978 under Sub-program 39-RT.

II. Justification of Basic Needs

A. C.E.E.R. New Wing present air conditioning system.

The air conditioning installation in the new wing of the Center for Energy and Environment Research (C.E.E.R.) was originally designed in 1968.

no. Power Flow Diagram during the Peak Hour Insolation, including Solar Cooling

#7. General Information for Economic Analyses

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Although some energy conservation features were included in the original design, application of more advanced know-how, and new technology can reduce the energy consumption in the building significantly.

The building houses basically laboratory facilities and office areas.

The actual components of the building envelope are:

Windows:

Solar bronze glass (22 percent of wall area).

Walls:

- a) Combination of insulated glass with concrete block back wall.
- b) Concrete with cement plaster.

Roof Area:

Concrete with 2" rigid insulation.

The main component of the actual air conditioning load is the fresh air load. In accordance with the original drawings, 20,600 CFM of outside air is supplied to the building as ventilation. This constitutes 65 percent of the total air circulation.

The peak design load was 200 TR and 50 percent of this load was outside air load.

A terminal reheat with hot water was included in the original design to maintain room conditions.

The existing air conditioning system consists of two chiller units, each having two 60-ton reciprocating compressors and two condenser fan units with a total installed capacity of 240 TR. The chiller provides chilled water to the air handling units and circulating system which comprise the remainder of the air conditioning system.

B. Existing system operation

The fresh air intake to the main air handling unit was blocked in order to reduce the outside air load. Actual building internal conditions, due to this action, are unpleasant, because the necessary fresh air for the laboratory hoods enters the building across windows, open doors, cracks and return duct openings as infiltration with a resulting high humidity room condition. The terminal reheat system is out of service completely. The central chilled water plant is always partially or totally out of service. The four existing compressors are Worthington Model EVC6-S2 and are of poor design. They have had a history of unreliability since first installed, being subject to multiple, internal breakdowns causing complete destruction of their interior mechanism. This has resulted in partial or complete loss of chilled water for the system, for periods of three to four months while parts were procured and repairs made.

The maintenance history of this plant shows that on an average two compressors have been down continuously, awaiting spare parts and repair over the past five years. Major plant breakdowns occurred in 1972 and in 1976 when all compressors were down for a period of four months each due to compressor failure. At that time it was necessary to augment the system with window-type air conditioners in laboratories where temperature-humidity sensitive equipment was being used.

The compressors have required the constant service of an air conditioning mechanic and the expenditure of large sums of money for maintenance and replacement parts to keep the system operational over the past six years. Maintenance problems have been compounded by the fact that the compressors are no longer manufactured, making spare parts difficult to find.

The following is a breakdown of expenditures made by the C.E.E.R. from operating funds to keep the chiller unit operational:

<u>Fiscal Year</u>	<u>Materials & Supplies</u>	<u>Air Cond. Tech. Salary</u>
1972	\$ 2,833	\$ 9,100
1973	8,628	9,100
1974	3,022	9,100
1975	9,933	9,100
1976	5,952	9,100
1977	<u>9,232</u>	<u>4,500</u>
Total	\$ 39,600	\$ 50,000
Grand Total		\$89,600

The annual cost of maintenance of this unit has taken such a large portion of the maintenance budget for the Bio-Medical building that it has been necessary to cut back on essential maintenance of the physical plant in order to have sufficient funds to keep the chiller unit operational. It is not considered economical or feasible to keep expending large amounts of money to repair a chiller system which is of inherently poor design and incapable of reliable operation.

The real loss is to the laboratory and treatment areas for the Nuclear Medicine Programs which require a continuous and reliable source of air conditioning in order to promote scientific research and patient comfort.

C. Electric energy consumption of the existing central chilled water plant.

An estimate of more than 40,000 KW H per month is actually used to operate just the central chilled water plant in the New Wing of the C.E.E.R. This electric energy with a total cost of more than \$2,800.00 per month is

used to operate a non-reliable system with the result of an uncomfortable environmental condition inside the building.

III. General Description of the Proposed Revision

A. Building upgrade for energy conservation.

In order to reduce the air conditioning load the following energy conservation measures seem to be imperative and are strongly recommended:

- 1) Provide all glass areas with Schochtint solar control film to minimize radiation load.
- 2) Provide inside venetian blinds for all windows.
- 3) Provide additional insulation at roof level with a three inch fiberglass matt above the hung ceiling at second floor.
- 4) Reduce the ventilation to the building. This can be accomplished by several ways as follows:
 - 4.1) Rebalance all supply and exhaust systems to the laboratory hoods to reduce the total air each system exhaust to the exterior.
 - 4.2) Reducing the ventilation air to other areas to the minimum recommended per the ASHRAE 90-75 and 62-73 standards.
 - 4.3) Provide an automatic control of the fresh air intake with static pressure sensors.
- 5) Make a total air rebalance and upgrading of the air side and controls.

- 6) Make a psychrometric study and provide controls as necessary in order to eliminate the reheat and maintain room conditions.

Items No. 1 and No. 2 above are already completed under an in-house conservation program.

Additional engineering is necessary to define the work of upgrading the building and the air conditioning system to provide a reduction to the refrigeration load.

B. Cooling load estimates for the "New Wing"

Using as a base the original set of construction drawings and considering the energy conservation features outlined in Section III, cooling load calculations for each month were performed. Load profiles were also prepared. The maximum hourly load was 113 TR at 4:00 p.m. for the average day in August. These calculations were prepared using the Automatic Procedures for Engineering Consultants, Inc. (APEC) program HCC-III. Attachment #1 and Attachment #2 include the computer print-out and the cooling load profiles, respectively. As indicated in the load profile chart for September 1978, a total of 917 TR x H/day are required to maintain building comfort conditions. The working day was considered from 8:00 a.m. to 5:00 p.m.

If we assume 250 working days per year and estimate the refrigeration work for the average day by the September data (i.e. 971 TR x H/day) the total yearly refrigeration work will be 197,750 TR x H/year or 697,941 KWH.

C- Concentrating Photovoltaic for the Tropics and its relation to the proposed revision

This project consists of a Solar Photovoltaic Concentrator Application for the Commonwealth of Puerto Rico. The application is unique in several aspects. First, it represents a total energy system designed to provide the electrical, cooling and thermal energy requirements of the Center for Energy and Environment Research (CEER) and hot water requirements of the adjacent Oncological and University Children's Hospitals, all located in the Medical Complex in San Juan. Second, the application will serve as a demonstration to Caribbean and Latin American Nations that solar energy in general and photovoltaics specifically can help them meet their energy needs while affording simultaneous relief from economic stress due to rising energy costs.

The project team consists of the Energy Office of the Commonwealth of Puerto Rico, Center for Energy and Environment Research of the University of Puerto Rico, TEAM, Inc. BHMG/Engineers, the AAI Corporation and Solarex Corporation.

The proposed system consists of a 20/1 concentrating first stage and a compound parabolic second stage with a concentration of about 2/1 to give an overall concentration ratio of 40/1. Solarex cells designed to operate with an efficiency of 10.9% at 100°C and 40 suns are to be incorporated into the second stage with a water cooling loop. The first stage utilizes flat segmented second surface glass mirrors in horizontal single axis east-west tracking mode. The expected overall array efficiency will be in the range 7.2-7.6%. The array has been sized at about 34,000 square feet of collectors to produce about 150 kW_e and about 1200 kW_{th} in form of hot water at 190°F.

The total electric peak power demand of CEER is about 425 kW_e. The major part of the load is the airconditioning (~85%). The electric and thermal energy generated by the photovoltaic array will be utilized to run a 70 ton electric direct expansion split system and two 120 ton absorption chillers respectively to meet the airconditioning demand of the CEER and to supply the hospitals with 110°F hot water.

The photovoltaic array will be interfaced in parallel with the utility (PRWRA) power grid through a line-commutated inverter to supply electrical power when there is not enough solar radiation. Excess power generated on holidays or otherwise will be fed back into the power grid and credited to CEER. This mode of operation eliminates the large investment and the maintenance cost associated with conventional batteries and represents a very useful and practical system where the utility grid replaces the storage.

This project in its first phase is one of the six projects of the concentrating type funded by DOE under the "Photovoltaics Technology Development and Applications Program." The overall objective of this program is "to bring the photovoltaic energy systems to the point where they are able to supply a significant portion of the nations energy requirements thus to reduce systems costs while at the same time resolving the technical, environmental and social issues involved in fostering widespread adoption of photovoltaic power systems."

D. Conceptual design schematic

In the solar collector piping diagram (Attachment #3) all elements indicated by single lines are parts of the photovoltaic project.

These are:

PHVA	-	Photovoltaic collector array
HWT	-	Hot water storage tank
P1	-	Solar collector water recirculation pump
SCS	-	Solar collector supply lines
SCR	-	Solar collector return lines
ACFC	-	Air cooled fluid cooler
SH	-	Steam heating coil

-Surge tank and hot water services to hospitals.

All elements indicated by double lines in the same diagram as well as all elements included in the chilled water and condensing water piping diagram (Attachment #4) are parts of this revision. These are:

ACH-1	-	Absorption chiller #1
ACH-2	-	Absorption chiller #2
P2-1	-	Hot water supply pump
P2-2	-	Hot water supply pump
HWS	-	Hot water supply lines
HWR	-	Hot water return lines
CT	-	Cooling tower
P3-1	-	Condensing water pump
P3-2	-	Condensing water pump
CHS	-	Chilled water supply lines

- CHR - Chilled water return lines
- CS - Condensing water supply lines
- CR - Condensing water return lines
- ACRCH - Air cooled reciprocating chiller

To provide a reliable system two (2) backup units are included as follows:

1. A steam heating coil (SH) will be included as part of the photovoltaic project inside the hot water storage tank (HWT) to provide hot water services to the hospitals in case of any failure in the solar array hot water system. This steam heating coil will also provide the back-up for the absorption air conditioning system when necessary.

2. One single air cooled reciprocating chiller (ACRCH) will be included as part of this project to provide the back-up based on electric energy in case of a failure in any of the absorption chillers or in the steam supply to the area.

E. Alternatives in case the Photovoltaic Project is not funded

In the case CEER does not receive the funding for the solar project the absorption chiller will be operated via a direct connection to the steam lines of the Medical Center. The existing steam distribution lines of the Central Steam Plant provide a simple connection port close to the location of the proposed absorption chillers. In this case a small modification of the generator will be necessary to operate the absorption chillers with steam. The use of absorption chillers energized by a steam supply from a large central steam plant is standard in the mainland U. S. A. The existing central steam plant at the Puerto Rico Medical Center is one of the largest in the Caribbean and has plenty excess capacity available.

The absorption chillers capacity will go up to 148 TR each when operated by direct steam. With this alternative one single absorption chiller will be able to handle the air conditioning load of the New Wing and the second unit will be ready for back-up purposes. In addition, the reciprocating chiller (ACRCH) will provide a second back-up in case of a failure in the steam supply to the area.

Based on the actual cost Medical Center charges CEER for the steam, the use of electrical cooling systems is in general more cost effective than using steam systems. However, for large uses of steam a new contract can be negotiated with the Medical Center to obtain a lower cost for the steam purchased.

F. System main components and their location

The main components of the photovoltaic project and of this project are shown in the plan of Attachment #5. The absorption chillers (ACH-1 and ACH-2), the hot water supply pumps (P2-1 and P2-2), all the controls for the chilled water system and the condensing water system will be located inside the existing machine shop building in an area to be prepared for this purpose. The cooling tower (CT), the condensing water pumps (P3-1 and P3-2), and the air cooled reciprocating chiller will be located inside the existing chiller area.

G. Thermal Energy available from the photovoltaic array to operate the absorption chillers.

1. Peak Hour Considerations:

As indicated in the Energy Flow diagram of Attachment #6, the thermal power available from the collector array at the peak average hour is 1021 KW. (3.47×10^6 BTU/H). If the proposed solar cooling system is utilized, 594 KW of this thermal power can be used to operate the absorption

chillers. With the use of this thermal power 126.8 Tons of refrigeration output can be obtained from an absorption chiller with a C.O.P. of 0.70. This is 112% of the peak hourly air conditioning load indicated in Section III-8 (113 T.R.).

2. Daily and Yearly Average Considerations:

Considering an average total direct radiation of 1300 BTU/sq. ft. per day, and a collector area of 3179.8 m² operating at 44% efficiency the available thermal energy per day is

$$T_{TD} = 5754 \text{ KW.H/day}$$

During the weekdays the hot water demand for the Oncologic and Pediatric Hospitals can be estimated as

$$T_{HD} = 2324 \text{ KW.H/day}$$

Thus the available thermal energy to operate the absorption chillers during a weekday is

$$T_{AD} = T_{TD} - T_{HD}$$

$$T_{AD} = 3430 \text{ KW.H/day}$$

For an estimated 250 working days per year the total available thermal energy to operate the air conditioning of the New Wing is:

$$T_{AY1} = 857,500 \text{ KW.H per year}$$

Additional energy will be available from the hot water storage tank (20,000 gallons) on monday mornings. During the weekend the photovoltaic array will operate without the thermal load of the solar cooling system and will maintain an average tank temperature close to 190°F. Thus a minimum of 83 KW.H will be available per weekend. For the 52 weekends of the year the energy available from the storage tank will be:

$$T_{AY2} = 33,124 \text{ KW H}$$

And the total for the year

$$T_{AY} = T_{AY1} + T_{AY2}$$

$$T_{AY} = 890,624 \text{ KW H per year}$$

In Section III-B the total energy necessary for a year of refrigeration in the New Wing was computed to be 697941 KW H/year. The Thermal Energy necessary for an absorption chiller system to provide this refrigeration can be estimated to be 897,000 KW.H/year. Thus the thermal waste energy from the photovoltaic array should provide 99% of the necessary refrigeration in accordance with above figures. However, some reduction in the solar contribution to the air conditioning system has to be considered because the air conditioning load profile and the profile of the energy available from the photovoltaic array are not identical. An 85% solar contribution to the air conditioning system can be considered as a reasonable estimate.

IV. Analysis of Safety and Pollution Aspects

The major safety hazards for this installation are fire and personal injuries. The origin of a fire could be from the electric motors of pumps and the air cooled chiller and associated electrical wiring and control panels. The control of a fire would be handled by providing CO₂ fire extinguishers in quick release mounts close to the equipment. Frequent inspections and checks by maintenance personnel would be made in this area to ensure all equipment is in good operating condition. These persons would be instructed in the method of shutting down the equipment and in the use of fire extinguishers for electrical fires. In addition, there are telephones available in the adjacent offices for calling the Fire Department, if needed.

Personnel injuries will be controlled by providing safety shields and guards around moving parts of the equipment. Personnel will be thoroughly instructed in the operation of the equipment, safety procedures and first aid.

The potential pollutants in this area would consist of liquid lithium bromide solution used as the absorbent in the absorption chiller unit and oil and grease used to service the pump and motors.

The lithium bromide is a non-toxic salt at standard atmospheric pressure and temperature. The refrigerant in the absorption cycle is distilled water. The charging of this system with lithium bromide would be done by trained personnel using proper equipment. Should an inadvertent spill happen, it will be quickly dispersed with a wash-down with soap and water and disposed of through the floor drain to the sewage system.

The proposed air cooled reciprocating chiller is a factory charged unit, and no freon leakage is expected from this one.

Oils and grease are kept in approved metal containers and stored in a metal locker when not being used. Oil spills will be cleaned with degreaser and washed down the floor drain with soap and water.

The proposed absorption chiller operation will reduce substantially the electric energy consumption of the system by the use of a non-polluting energy, i.e. solar energy. The overall effect on the environment of the island of Puerto Rico will be a reduction in pollution.

V. Consideration Given to the Use of Existing Facilities

The existing chiller units will be eliminated. The rest of the existing air conditioning installation will be maintained in service with small modifications to upgrade the operation.

VI. Proposed equipment specifications

ACH-1, ACH-2 ABSORPTION CHILLER

- A) Nominal capacity: 148 TR
- B) Actual capacity for low temperature application: 63.4 TR
- C) Generator:

 Passes: 2

 Flow: 320 GPM

 Inlet Temperature: 190°F

 Outlet Temperature: 182.5°F

- D) Condensing Water:

 Flow: 353 GPM

 Inlet Temperature: 85°F

 Outlet Temperature: 95°F

- E) Chilled Water:

 Flow: 160 GPM

 Inlet Temperature: 55°F

 Outlet Temperature: 45°F

- F) Power Input: (4.2 kw)

Trane model ABSC-01E or similar

CT COOLING TOWER

- A) Capacity to cool 353 GPM of water from 95°F to 85°F at 80°F wet bulb outside temperature.

- B) Power input 7-1/2 HP (6.6 kw)

Baltimore Air Coil (BAC) CFT 2413 or similar

ACRCH AIR COOLED RECIPROCATING CHILLER

- A) Capacity 69.9 TR with 90°F entering air at condenser and 45°F leaving chilled water temperature.

- B) Total power input 83.1 KW.
 C) Trane CG AA 7506 E or similar.

VII. Preliminary Cost Estimate

Project C.E.E.R. New Wing Air Conditioning Upgrading

I- Mechanical Equipment

1	Absorption chillers	ea.	2	38,000.-	76,000.00
2	Air cooled chiller	ea.	1	21,000.-	21,000.00
3	Cooling Tower	ea.	1	9,000.-	9,000.00
4	Hot water supply powers	ea.	2	1,500.-	3,000.00
4	Condensing water supply pumps	ea.	2	2,000.-	4,000.00
Mechanical Equipment Total					\$ 113,000.00

II- Mechanical-Electrical Contract

No.	Description	Unit	Quantity	Unit Price	Total
1	Equipment installation	LS	1	5,000.00	5,000.00
2	5" chilled water lines with 1" methane insulation	LF	200	25.00	5,000.00
3	5" Condensing water lines	LF	200	19.00	3,800.00
4	8" Condensing water lines	LF	100	30.00	3,000.00
5	4" Hot water lines with 2" methane insulation	LF	120	20.00	2,400.00
6	Connections to existing chilled water lines	LS			1,000.00

II- Mechanical-Electrical Contract

No.	Description	Unit	Quantity	Unit Price	Total
7	Cooling tower and c.w.pumps connection	LS			1,000.00
8	Absorption chillers and hot water pumps connections	LS			2,000.00
9	Upgrade existing air conditioning installation	LS			10,000.00
10	Modifications in shop Building	LS			5,000.00
11	Insulation addition to roof level. 3" Fiber glass	SF	10,000	1.00	10,000.00
12	Safety switch and power electrical conn. for absorption units	EA	2	500.00	10,000.00
13	Safety switch and power electrical conn. for reciprocating chiller	EA	1	\$1,000.00	\$ 1,000.00
14	Combination magnetic starters and power electrical conn. for hot water pumps	EA	2	700.00	1,400.00
15	Combination magnetic starters and power electrical conn. for cooling tower and cond. water pumps	EA	3	1,000.00	3,000.00
16	Air handling unit and duct work upgrading	LS	1		5,000.00

II- Mechanical-Electrical Contract

No.	Description	Unit	Quantity	Unit Price	Total
17	Hot water and chilled water system upgrading	LS	1		5,000.00
18	Systems balance and test	LS			4,000.00
19	Air conditioning system control upgrading	LS	1		8,000.00
20	Control chilled water plant controls	LS	1		2,000.00
Subtotal					\$ 78,600.00
30% Overhead, Profit and Taxes					23,500.00
Total					<u>\$102,100.00</u>

SUMMARY OF PRELIMINARY COST ESTIMATE

No.	Description	Unit	Quantity	Unit Price	Total
I	Mechanical Equipment				\$ 113,000.00
II	Mechanical Electrical Contract				<u>102,180.00</u>
	Sub-total				\$ 215,180.00
III	10% Contingencies on Mechanical Equipment				11,300.00
IV	20% Contingencies on Mechanical Electrical Contract				<u>20,436.00</u>
	Sub-total				\$ 246,916.00
V	Engineering and Project management at 12% of items #1 & #2				<u>25,814.00</u>
	Total				\$ 272,730.00

VIII. Comparative Economic Analysis between the Previous Proposal of April, 1977 and the Present Proposal.

This economic analysis is included in order to underline the cost effectiveness of the present revised proposal.

The initial investment for this project is higher than the estimated investment for the previous proposal. However, "Uniform Annual Cost" is substantially lower due to the use of the waste thermal energy from the photovoltaic array.

Basic Data for the Preliminary Proposal of April 1977 (Alternative A)

. New oil-cooled centrifugal chiller (270 TR) with steam terminal reheat	
. Estimated design and inspection cost:	\$ 17,629.00
. Estimated project cost (investment):	164,000.00
. Escalation two years at 5% per year:	16,450.00

. Upgrading of air distribution system, reheat system and controls:	\$ 12,500.00
. Estimated Steam Cost, 526,000 lb/year at \$17/1000 lb:	3,682.00
. Estimated yearly refrigeration:	3.5 x 10 ⁵ TR.H
. Estimated electric energy to operate the air cooled centrifugal chiller to provide this refrigeration set 1.3 KW per TR:	4.55 x 10 ⁵ KWH
. Estimated first year cost at \$.07 per KW H:	\$ 31,850.00
. Estimated first year cost for maintenance, spare parts, etc.:	\$ 4,000.00
. Calculated uniform annual cost without terminal value over 20 years life time. For more detail see computer print out "Alternative A" :	\$ 140,292.40

Basic Data for the Revised Proposal, February 1979 (Alternative B)

. Solar energized absorption chillers each 148 TR	
. Estimated design and project management cost:	\$ 25,814.00
. Estimated project cost (investment):	\$ 246,916.00
. Upgrading of air distribution system and controls:	
. Estimated steam cost, 263,000 lb/year at \$7/1000 lb:	\$ 1,841.00
. Estimated electrical energy to operate the absorption chillers auxiliary equipment and the air cooled refrigeration chiller to provide 15% of the cooled:	1.06 x 10 ⁵ KWH
. Estimated first year cost at \$.07 per KW.H:	\$ 7,420.00
. Estimated first year cost for maintenance, spare parts, etc.:	\$ 4,000.00
. Calculated Uniform annual cost without terminal value over 20 years life time. For more detail see computer print out for "Alternative B":	\$ 63,488.61

Computations on both alternatives (A and B) show clearly the significant economical advantage of the solar cooling. The uniform annual cost difference is about \$76,804. Over a life time of twenty years without the terminal value the relative savings will be \$1,536.080 in 1978 dollars.

In terms of relative pay back* the solar system will pay back in less than 3 years.

* We define relative pay back as follows:

The time during which the summation of the difference in recurring costs equals the difference in non-recurring cost of the first year.

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ECONOMIC ANALYSIS

DATE- FEBRUARY 5, 1979
 PROJECT- CEFR CWA -8495
 SUBJECT- NEW WING AIR CONDITIONING AND GRADING
 DESCRIPTION- COMPARATIVE ANALYSIS BETWEEN 1977 AND 1979 PROPOSALS
 ALTERNATIVE- A-PROPOSAL OF APRIL 1977

ECONOMIC CONSIDERATIONS- 20 YEAR LIFE

10.0 PERCENT INTEREST RATE
 12.0 PERCENT STEADY ESCALATION RATE
 15.0 PERCENT ELECTRICAL ENERGY ESCALATION RATE
 2.0 PERCENT OTHER ESCALATION RATE
 \$ 0.00 TERMINAL VALUE

YEAR	MANAGEMENT	INVESTMENT	STEADY	ELECTRICAL ENERGY	OTHER	TOTAL	ALL COSTS	DISCOUNT FACTOR	DISCOUNTED COST
1	1742.00	18301.00	3687.00	31883.00	2080.00	37533.00	238168.00	0.9545	777342.14
2	0.00	0.00	4121.60	36627.50	2040.00	42789.10	42789.10	0.9677	37131.53
3	0.00	0.00	4616.19	42121.62	2080.00	48988.61	48988.61	0.7808	38512.75
4	0.00	0.00	5170.13	48439.86	2122.41	55732.41	55732.41	0.7171	39963.29
5	0.00	0.00	5798.55	55705.94	2164.86	63661.26	63661.26	0.6619	41513.36
6	0.00	0.00	6485.41	64061.72	2209.16	72755.90	72755.90	0.5926	43121.89
7	0.00	0.00	7263.66	73670.98	2252.32	83186.97	83186.97	0.5308	44827.47
8	0.00	0.00	8135.30	84721.63	2297.37	95154.31	95154.31	0.4898	46633.68
9	0.00	0.00	9111.64	97429.87	2343.31	108884.74	108884.74	0.4453	48466.64
10	0.00	0.00	10204.62	112044.35	2390.18	124639.47	124639.47	0.4048	50456.51
11	0.00	0.00	11429.52	128881.01	2437.98	142719.52	142719.52	0.3660	52523.87
12	0.00	0.00	12801.06	148179.66	2486.74	163466.47	163466.47	0.3345	54880.79
13	0.00	0.00	14337.10	170605.44	2536.48	187279.13	187279.13	0.3041	5684.51
14	0.00	0.00	16057.65	195864.28	2587.21	214611.15	214611.15	0.2764	5931.51
15	0.00	0.00	17894.57	225381.22	2634.05	245984.75	245984.75	0.2513	6181.13
16	0.00	0.00	20142.72	259165.41	2681.73	281999.86	281999.86	0.2285	64437.95
17	0.00	0.00	22559.84	299040.22	2745.57	323345.64	323345.64	0.2077	67177.82
18	0.00	0.00	25267.03	347466.25	2800.48	370813.76	370813.76	0.1888	70020.82
19	0.00	0.00	28299.07	404159.19	2856.49	425313.75	425313.75	0.1716	73010.31
20	0.00	0.00	31694.06	459381.92	2913.62	487890.50	487890.50	0.1561	76147.91
21									
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49									
50									

DISCOUNTED TOTAL COST \$ 1254107.73
 DISCOUNTED TERMINAL VALUE ... \$ 0.00

NET DISCOUNTED TOTAL COST ... \$ 1254107.73

UNIFORM ANNUAL COST WITHOUT TERMINAL VALUE ... \$ 140292.40
 UNIFORM ANNUAL COST WITH TERMINAL VALUE \$ 140292.40

CAPACETE, VARTIA & ASSOCIATES ENGINEERS-ARCHITECTS
 POST OFFICE BOX 9684
 SANTURCF, PUERTO RICO 00984 (809) 782-4144

E C O N O M I C A N A L Y S I S

DATE- FEBRUARY 9, 1979
 PROJECT- CEER CVA -8495
 SUBJECT- NEW KING AIR CONDITIONING UP GRADING
 ALTERNATIVE- R-REVISED PROPOSAL OF FEBRUARY 1979

ECONOMIC CONSIDERATIONS- 20 YEAR LIFE
 10.0 PERCENT INTEREST RATE
 12.0 PERCENT STEAM ESCALATION RATE
 15.0 PERCENT ELECTRICAL ENERGY ESCALATION RATE
 2.0 PERCENT OTHER ESCALATION RATE
 \$ 0.00 TERMINAL VALUE

YEAR	MANAGEMENT	INVESTMENT	STEAM	ELECTRICAL ENERGY	OTHER	TOTAL	DISCOUNT FACTOR	DISCOUNTED COST
1	25814.00	246916.00	1841.00	7457.30	4000.00	13298.00	0.9545	273026.72
2	0.00	0.00	2061.92	8575.55	4080.00	14717.47	0.8677	12771.95
3	0.00	0.00	2309.35	9861.84	4161.60	16332.83	0.7898	12884.64
4	0.00	0.00	2586.47	11341.16	4244.83	18172.46	0.7171	13032.64
5	0.00	0.00	2856.84	13042.33	4329.72	20268.91	0.6519	13214.47
6	0.00	0.00	3244.47	14998.69	4416.32	22659.48	0.5926	13437.22
7	0.00	0.00	3633.80	17248.49	4504.64	25386.95	0.5388	13573.49
8	0.00	0.00	4069.86	19835.76	4594.74	28500.37	0.4898	13547.41
9	0.00	0.00	4589.24	22811.13	4686.63	32056.01	0.4453	14274.62
10	0.00	0.00	5105.23	26232.80	4780.37	36118.41	0.4048	14621.67
11	0.00	0.00	5717.84	30167.77	4875.97	40761.56	0.3680	15071.71
12	0.00	0.00	6404.01	34692.88	4973.49	46070.39	0.3345	15413.61
13	0.00	0.00	7172.49	39896.81	5072.95	52142.27	0.3041	15758.94
14	0.00	0.00	8032.19	45881.33	5174.42	59088.95	0.2764	16237.45
15	0.00	0.00	8997.17	52763.53	5277.91	67038.62	0.2513	16753.73
16	0.00	0.00	10076.83	60678.06	5383.47	76138.37	0.2285	17398.42
17	0.00	0.00	11286.05	69779.77	5491.14	86556.97	0.2077	17981.07
18	0.00	0.00	12668.38	80266.74	5600.86	98488.09	0.1889	18598.84
19	0.00	0.00	14157.22	92283.75	5712.98	112193.96	0.1716	19254.97
20	0.00	0.00	15856.09	106126.31	5827.24	127809.65	0.1550	19547.59
DISCOUNTED TOTAL COST							\$ 567540.09	
DISCOUNTED TERMINAL VALUE ...							\$ 0.00	
NET DISCOUNTED TOTAL COST ...							\$ 567540.09	

UNIFORM ANNUAL COST WITHOUT TERMINAL VALUE ... \$ 63488.61
 UNIFORM ANNUAL COST WITH TERMINAL VALUE ... \$ 63488.61

IX. Design and construction schedule

The U. S. DOE will announce the winners of the Second Phase of the Concentrating Photovoltaic Projects around the first of May, 1979. It is imperative for the C.E.E.R. to receive the final decision by the Oak Ridge Operations Offices on the revision at least one month prior to that date, i.e. by April 1, 1979.

The proposed design and construction schedule for the uprating of the New Wing air conditioning system follows:

- | | | | | |
|-----------|---|-------------|---|--|
| April 2 | - | April 16 | - | Choose an Engineering/Architect firm to perform the design and project management. |
| April 16 | - | April 23 | - | Complete final equipment selection. Request equipment quotations. |
| April 23 | - | April 30 | - | Select equipment supplier and prepare purchase orders. |
| April 16 | - | May 7 | - | Prepare final construction drawings and prepare bidding documents. |
| May 7 | - | May 28 | - | Contractor bidding time and contract award |
| May 28 | - | August 6 | - | Construction time |
| August 6 | - | August 20 | - | Receive chillers and install |
| August 20 | - | September 3 | - | System balance, test and acceptance. Ready to interface with photovoltaic array. |

X. Conclusions

A. Reliability

The proposed revision will provide a more reliable system than the proposal of April 1977. The absorption refrigeration units have practically no moving parts. One small hermetic pump is the only moving part in these

chillers. In contrast to that the proposal of April 1977 involves a large centrifugal chiller with a rotor-impeller assembly moving at 8000 RPM.

The revised proposal as detailed in section III-d will include two different back-up systems. The proposal of April 1977 considered the re-use of the existing reciprocating units as back-up. According to the same proposal this equipment is of poor design, and has had a history of unreliability since the first day it was installed. The compressors for these units are no longer manufactured and to find parts is almost impossible.

B. Cost effectiveness

The comparative "Economic Analysis" included in Section VIII indicates that the new proposal is more cost effective than the previous proposal.

C. Energy conservation

A dramatic reduction in electric energy consumption of C.E.E.R. will be obtained with the revised proposal.

D. Pollution aspects

The use of non-polluting solar energy to operate the system will be a step towards improving the overall environmental condition on the island of Puerto Rico.

E. System completeness

With the provisions included in the proposal of April, 1977 the attempt of upgrading the C.E.E.R. New Wing air conditioning system would be incomplete. An improvement of the existing conditions inside the building should be a part of the overall effort. This revised proposal includes the improvement of the conditions inside the building.

F. Energy savings

Substantial energy savings will be obtained with the revised proposal. A yearly total of 3.44×10^5 KW H of electrical energy can be saved

with the solar air conditioning.

G. Total savings over the 20 years life time

Total savings over the 20 years life time of the solar equipment will exceed 1.5 Millions in 1978 dollars.

ATTACHMENT #1

C.E.E.R. NEW WING BUILDING
HOURLY COOLING LOAD ESTIMATES

C.E.E.R. New Wing
Building Hourly Cooling Load Estimates

Summary

	<u>Page</u>
C.E.E.R. - NW-1 January	1
C.E.E.R. - NW-2 February	8
C.E.E.R. - NW-3 March	11
C.E.E.R. - NW-4 April	14
C.E.E.R. - NW-5 May	17
C.E.E.R. - NW-6 June	20
C.E.E.R. - NW-7 July	23
C.E.E.R. - NW-8 August	26
C.E.E.R. - NW-9 September	29
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C.E.E.R. N.W - 1

Automated Procedures for Engineering Consultants, Inc.

HVAC CALCULATION, HCC-III(02) - CAPACITE - MARTIN AND ASS. SAN JUAN, PR.

PROJECT - 8488 CENTER FOR ENERGY & ENVIRONMENT RESEARCH 10/12/78 PAC

WEATHER PROFILES

MONTH	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20
TEMPERATURE, DB	71.0	73.0	76.0	80.0	82.0	83.0	83.0	83.0	82.0	81.0	80.0	79.0	78.0	77.0	76.0	75.0	74.0	73.0	72.0	71.0
TEMPERATURE, WB	67.8	69.7	71.1	73.0	74.5	74.6	74.2	73.6	73.4	72.9	73.2	72.9	72.9	72.9	72.9	72.9	72.9	72.9	72.9	72.9
WIND VELOCITY, MPH	139	149	153	159	167	166	162	157	156	154	159	157	157	157	157	157	157	157	157	157

GEOGRAPHIC/SOLAR DATA

INWARD FLOW FRACTIONS

LATITUDE	18.44	NI	NIU	NIR										
GROUND REFLECTIVITY	0.20	0.33	0.00	0.00										
CLEARNESS FACTOR	1.00													
MAX. SOLAR GAIN, BTUH/SF	80.00	DAYLIGHT SVG.	J	F	Y	A	N	J	J	A	S	O	N	O
DEGS. FROM STD. MERIDIAN	-5.00	IN-EFFECT	0	0	0	0	0	0	0	0	0	0	0	0

DESIGN CONDITIONS

MASTER-BUILDING DATA

	WINTER	SUMMER		
INSIDE TEMPERATURE	76.0	76.0	BLDG. ORIENT.	65.0 DEG. CORR. FACT.
RELATIVE HUM	50.0	55.0	WALL HEIGHT	26.80 FEET
HUMIDITY RAT	0.0096	0.0106	HOUR AVERAGE	5
OUTSIDE TEMPERATURE, DB	0.0	83.0	COOLING D.T.	20.0 DEG.
TEMPERATURE, WB	0.0	74.6	HEATING D.T.	50.0 DEG.
MONTH	1	1	HEATING LOAD	NO
			COOLING LOAD	YES
			OMIT WINT. SUN	NO
			CIRCN. RATE	0.00 AC/HR, MIN
			COIL R.P. FAC.	0.10
			R.A. PLENUMS	NO
			CALC. APP	NO

OCCUPANCY

LIGHTING

RTU/PERSON, SENS.	255	WATTS/SF	9.80
RTU/PERSON, LAT.	255	LOAD PROFILE NO.	2
LOAD PROFILE NO.	1	PERCENT TO R.A.	0
SF/PERSON	0.00		
MAX. NO. OF PEOPLE	40		

LOAD FACTOR MULTIPLIERS

AIR QUANTITY FACTORS

LIGHTS	0.80	JOB SITE ALTITUDE	0 FT
APPLIANCES	0.50	BAROMETRIC PRESSURE	29.921
PEOPLE	0.80	AIR DENSITY FACTOR	1.000
PUMP HEAT	1.00		

VENTILATION

INFILTRATION

CFM/SF	0.50	AIR CHANGE/HR	0.00
CFM/PERSON	10.00	DIVERSITY FACTOR	0.80
AIR CHANGE/HR	2.60		
PCT. FAN CFM	0.00		

1 2 3 4 5 6 7 8
 RUN OPTIONS USED 0 0 1 0 0 1 0 1

AUTOMATED PROCEDURES FOR ENGINEERING CONSULTANTS, INC.

HVAC CALCULATION (ACC-III(2)) CAPACITE-MARTIN AND ASS. SAN JOAQUIN, CA.

PROJECT - #495 CENTER FOR ENERGY & ENVIRONMENT RESEARCH 10/12/79 PAGE

ZONE DESCRIPTION DATA

ZONE NUMBER 100 CENTER FOR ENERGY

INSIDE DESIGN CONDITIONS

WINTER SUMMER

INSIDE

TEMPERATURE 76.0 76.0
RELATIVE HUM 50.0 55.0
HUMIDITY RAT 0.0086 0.0106

MASTER ZONE DATA

WALL HEIGHT 26.80 FEET
COOLING D.T. 20.0 DEG.
HEATING D.T. 50.0 DEG.
HEATING LOAD NO
COOLING LOAD YES
CIRCN. RATE 0.00 AC/HR. MIN
R.A. PLEXIMS NO
CALC. APP NO

OCCUPANCY

BTU/PERSON, SENS. 255.
BTU/PERSON, LAT. 255.
LOAD PROFILE NO. 1
SF/PERSON 0.00
MAX. NO. OF PEOPLE 40

LIGHTING

WATTS/SF 9.80
LOAD PROFILE NO. 2
PERCENT TO R.A. 0.

LOAD FACTORS

LIGHTS 0.80
APPLIANCES 0.50
PEOPLE 0.80
SAFETY FAC. 1.00
DUCT HEAT 1.00

VENTILATION

FIXED CFM 13000.00
CFM/SF 0.50
CFM/PERSON 10.00
AIR CHANGE/HR 2.60
DCT. FAN CFM 0.00

SYSTEM ANALYSIS

SUPPLY FAN STATIC 2.50 IN. W.G.
RETURN FAN STATIC 0.00 IN. W.G.
O.A. FAN STATIC 0.00 IN. W.G.
AIR SYSTEM TYPE - MIXED AIR
FAN LOCATION - DRAW THRU
COIL BYPASS FACTOR 0.10

AUTOMATED PROCEDURES FOR ENGINEERING CONSULTANTS, I.C.

HVAC-CALCULATION-HCC-1H(12) CARACITE-MARTIN AND ASS. SAN JUAN, PR.

PROJECT - 8485 CENTER FOR ENERGY & ENVIRONMENT RESEARCH 10/12/78

INTERNAL LOAD PROFILES -- PER CENT OF PEAK VALUE

PROFILE NO. 1

HOUR	1	2	3	4	5	6	7	8	9	10	11	12
LOAD	0.	0.	0.	0.	0.	0.	0.	100.	100.	100.	100.	85.

HOUR	13	14	15	16	17	18	19	20	21	22	23	24
LOAD	100.	100.	100.	100.	100.	0.	0.	0.	0.	0.	0.	0.

PROFILE NO. 2

HOUR	1	2	3	4	5	6	7	8	9	10	11	12
LOAD	0.	0.	0.	0.	0.	0.	0.	100.	100.	100.	100.	85.

HOUR	13	14	15	16	17	18	19	20	21	22	23	24
LOAD	100.	100.	100.	100.	100.	0.	0.	0.	0.	0.	0.	0.

AUTOMATED PROCEDURES FOR ENGINEERING CONSULTANTS, INC.

HVAC CALCULATION, HCC-1111(2) CAPACITE-MARTIN AND ASS. SAN JUAN, PR.
 PROJECT - 8495 CENTER FOR ENERGY & ENVIRONMENT RESEARCH 10/12/78 PAGE

EXTERIOR WALLS

TYPE NUMBER	WALL DESCRIPTION	DECREMENT FACTOR	TIME LAG	COLOR	U-FACTOR		BELOW GRAD RTU/SF
					SUMMER	WINTER	
1	9 IN CONCRETE WALL	0.91	6.	L	0.51	0.51	0.0
2	WALL COMBINATION	0.20	8.	L	0.06	0.06	0.0

ROOFS

TYPE NUMBER	ROOF DESCRIPTION	DECREMENT FACTOR	TIME LAG	COLOR	U-FACTOR	
					SUMMER	WINTER
1	6 IN CONCRETE-5IN INSU	0.20	8.	L	0.06	0.06

CEILINGS

TYPE NUMBER	CEILING DESCRIPTION	CEILING U-FACTOR	ROOF ABOVE		FLOOR ABOVE	
			TYPE	TEMP	TYPE	WIN TEMP

PARTITIONS

TYPE NUMBER	PARTITION DESCRIPTION	U-FACTOR	UN-CONDITIONED SPACE TEMPERATURE	
			SUMMER	WINTER

FLOORS

TYPE NUMBER	FLOOR DESCRIPTION	U-FACTOR	TEMP. UN-COND. SPACE		BELOW GRD RTU/SF	ON GRI RTU/LF
			SUMMER	WINTER		

EXTERIOR DOORS

TYPE NUMBER	DOOR DESCRIPTION	U-FACTOR	AREA SF	INFILTRATION
				CFM (WINTER)

AUTOMATED PROCEDURES FOR ENGINEERING CONSULTANTS, INC.

HVAC CALCULATION (HCC-111102) - CAPACITE-MARTIN AND ASS. SAN JUAN, PR.

PROJECT - 8485 CENTER FOR ENERGY & ENVIRONMENT RESEARCH 10/12/78 PAGE

WINDOWS

TYPE NUMBER	WINDOW DESCRIPTION	GLASS DIMENSIONS			U-FACTORS			PCT. DESS		SKL PCT
		TYPE	HGT	WTH	SHADE	SUN	WATR	OPER	VERT	
1	SOLAR BROWN-SCOTCH TINT	15	5.0	9.0	0.81	1.10	0.81	82.	90.	0
2	SOLAR BROWN-SCOTCH TINT	15	6.0	9.0	0.81	1.10	0.81	82.	90.	0

TYPE NUMBER	SHADE COEFFICIENTS	AIR SUPPLY	OVERHANG AND FIN				VERT. PROJ.	ABOVE BOTTOM	SHADE TYPE
			TOTAL ABOVE TOP	BEYOND LEFT	BEYOND RIGHT	DEPTH			
1	0.31 GL	0 U	0.0	0.00	0.00	0.00	0.0		OV
	0.00 INS	0 R	0.0	0.00	0.00		0.0		LF
	0 SCR		0.0	0.00		0.00		0.0	RF
2	0.31 GL	0 U	0.0	0.00	0.00	0.00	0.0		OV
	0.00 INS	0 R	0.0	0.00	0.00		0.0		LF
	0 SCR		0.0	0.00		0.00		0.0	RF

CODES

- GL SPECIAL GLASS SHADING COEFFICIENT
- INS INSIDE SHADING COEFFICIENT (1.00=NO SHADING)
- SCR EXTERIOR SUNSCREEN TYPE
- AIR SUPPLY U=AIR SUPPLIED UNDER WINDOW (1=YES)
R=AIR SUPPLIED BETWEEN WINDOW AND DRAPES
- VERT. PROJ. DEPTH OF OVERHANG VERTICAL PROJECTION
- ABOVE BOTTOM DISTANCE ABOVE BOTTOM OF WINDOW TO BOTTOM OF FIN
- LF AND RF LEFT FIN AND RIGHT FIN (VIEWED FROM OUTSIDE)
- OV ROOF OVERHANG

AUTOMATED PROCEDURES FOR ENGINEERING CONSULTANTS, INC.

HVAC CALCULATION, HCC-111(02) - CARACETE-MARTIN AND ASS. SAN JUAN, PR.

PROJECT - 8495 CENTER FOR ENERGY & ENVIRONMENT RESEARCH 10/12/78 PAGE 1

BUILDING LOADS SUMMARY

	HEAT GAIN - COOLING		HEAT LOSS	
	SENSIBLE	LATENT	HEATING	WINTER GAIN
WINDOW TRANS	12866.		0.	
WINDOW SOLAR	46103.			0.
WALL	11475.		0.	
ROOF/CEILING	764.		0.	
PARTITION	0.		0.	
FLOOR	0.		0.	
DOOR	0.		0.	
INFILTRATION	0.	0.	0.	
LIGHTS	267076.			267076.
PEOPLE (31)	8423.	8423.		8423.
APPLIANCES	87000.	0.		87000.
TOTALS	433710.	8423.	0.	362499.
TOTAL HEAT	442133.		PLMM HT	0.
AT PEAK HOUR	13		VENT.	136136.
SENS. HEAT RATIO	0.98		TOTAL HUMID	136136.
LIGHT HEAT TO P.A.		0.		13.6 BTUH/SF
SKYLIGHT HEAT TO P.A.		0.		
VENTILATION CFM	13000.			363792. HEATING+HUMID
EXHAUST CFM	0.			
PUMP HEAT FACTOR		1.00		
BUILDING REFRIGERATION LOAD		1025493.		
TONS OF REFRIGERATION		85.		

REFERENCE VALUES

	AREA	VOLUME	RTUH/SF COOL HEAT	RTUH/CF COOL HEAT	SF PER TON	PER MBH	CFM/SF COOL
COOLING	9990.	267732.	102.7	3.8	117.5		2.7
HEATING	0.	0.	0.0	0.0		0.0	
TOTAL BLDG	9990.	267732.	102.7	3.8	117.5	73.4	2.7

AUTOMATED PROCEDURES FOR ENGINEERING CONSULTANTS, INC.

HVAC CALCULATION, HCC-III(02) - CAPACITE - MARTIN AND ASS., SAN JUAN, PR.

PROJECT - BASE CENTER FOR ENERGY & ENVIRONMENT RESEARCH 10/12/78 PAGE 2

BUILDING HOURLY COOLING LOADS (*-BLDG. REFG. INCLUDES VENTILATION)

HOOR	8	9	10	11	12	13
SENSIBLE						
WIN TRANS	9190.	5514.	0.	7352.	11028.	12866.
WIN SOLAR	41431.	57107.	61184.	59463.	54503.	46103.
WALL	14236.	12860.	11485.	11480.	11475.	11475.
ROOF/CEILING	1701.	1092.	982.	873.	764.	764.
FLOOR	0.	0.	0.	0.	0.	0.
DOOR	0.	0.	0.	0.	0.	0.
INFILT	0.	0.	0.	0.	0.	0.
LIGHT TO RM	267076.	267076.	267076.	267076.	227015.	267076.
PEOPLE	8423.	8423.	8423.	8423.	7159.	8423.
APPLIANCE	87000.	87000.	87000.	87000.	73949.	87000.
TOTAL (INCL. PARTITIONS)	410178.	428045.	436152.	441669.	385896.	433710.
LATENT						
INFILT	0.	0.	0.	0.	0.	0.
PEOPLE	8423.	8423.	8423.	8423.	7159.	8423.
APPLIANCE	0.	0.	0.	0.	0.	0.
TOTAL	8423.	8423.	8423.	8423.	7159.	8423.
TOTAL LOAD	418601.	436469.	444575.	450092.	393056.	442133.
BLDG REFG. *	581323.	777493.	843846.	940056.	946260.	1025493.
	57	65	70	79	78	85
HOOR	14	15	16	17	18	19
SENSIBLE						
WIN TRANS	12866.	12866.	12866.	11028.	9190.	7352.
WIN SOLAR	34905.	22488.	11662.	4652.	0.	0.
WALL	31912.	40130.	43972.	46335.	48446.	50407.
ROOF/CEILING	764.	764.	1854.	3332.	4706.	5889.
FLOOR	0.	0.	0.	0.	0.	0.
DOOR	0.	0.	0.	0.	0.	0.
INFILT	0.	0.	0.	0.	0.	0.
LIGHT TO RM	267076.	267076.	267076.	267076.	0.	0.
PEOPLE	8423.	8423.	8423.	8423.	0.	0.
APPLIANCE	87000.	87000.	87000.	87000.	0.	0.
TOTAL (INCL. PARTITIONS)	442948.	438750.	432855.	427849.	62344.	63648.
LATENT						
INFILT	0.	0.	0.	0.	0.	0.
PEOPLE	8423.	8423.	8423.	8423.	0.	0.
APPLIANCE	0.	0.	0.	0.	0.	0.
TOTAL	8423.	8423.	8423.	8423.	0.	0.
TOTAL LOAD	451371.	447173.	441279.	436272.	62344.	63648.
BLDG REFG. *	1017351.	884738.	971235.	937239.	356401.	331737.
	84	82	81			

$\sum = 681 \text{ TR. H.}$
14

C.E.E.R. NW-2

8

AUTOMATED PROCEDURES FOR ENGINEERING CONSULTANTS, INC.

HVAC CALCULATION, MCC-III(02) - CAPACETE-MARTIN AND ASS. SAN JUAN, PR.

PROJECT - 8495 CENTER FOR ENERGY & ENVIRONMENT RESEARCH 10/12/78 PAGE 1

WEATHER PROFILES

HOURS	10	11	12	13	14	15	16	17	18	19	
MONTH 1	71.0	73.0	76.0	80.0	82.0	83.0	83.0	82.0	81.0	80.0	DB
	67.0	68.7	71.1	73.0	74.6	74.6	74.2	73.6	73.4	72.9	WB
	139	140	153	159	167	166	162	157	156	154	HP X 1000
MONTH 2	73.0	76.0	79.0	81.0	83.0	84.0	84.0	83.0	82.0	81.0	DB
	71.3	72.7	72.9	73.3	74.4	74.9	74.9	75.0	74.1	73.4	WB
	162	166	163	159	164	166	166	167	159	156	HP X 1000

GEOGRAPHIC/SOLAR DATA

LATITUDE	18.44
GROUND REFLECTIVITY	0.20
CLEARNESS FACTOR	1.00
MAX. SOLAR GAIN, BTUH/SF	80.00
DEGS. FROM STD. MERIDIAN	-5.00

INWARD FLOW FRACTIONS

NI	MIU	NIU
0.33	0.00	0.00
DAYLIGHT SVGS. J F M A M J J A S O N D		
IN EFFECT 0 0 0 0 0 0 0 0 0 0 0 0		

DESIGN CONDITIONS

	WINTER	SUMMER
INSIDE TEMPERATURE	76.0	76.0
RELATIVE HUM	50.0	55.0
HUMIDITY RAT	0.0006	0.0106
OUTSIDE TEMPERATURE, DB	0.0	84.0
OUTSIDE TEMPERATURE, WB	0.0	75.0
MONTH	1	2

MASTER BUILDING DATA

BLDG. ORIENT.	65.0 DEG.	CORR. FACT.
WALL HEIGHT	26.80 FEET	
POW. AVERAGE	5	
COOLING D.T.	20.0 DEG.	
HEATING D.T.	50.0 DEG.	
HEATING LOAD	NO	
COOLING LOAD	YES	
OMIT WINT. SUN	NO	
CIRCN. RATE	0.00 AC/HP, MIN	
COIL R.P. FAC.	0.10	
R.A. PLENUMS	NO	
CALC. ADP	NO	

OCCUPANCY

RTU/PERSON, SENS.	255
RTU/PERSON, LAT.	255
LOAD PROFILE NO.	1
SE/PERSON	0.00
MAX. NO. OF PEOPLE	40

LIGHTING

WATTS/SF	9.80
LOAD PROFILE NO.	2
PERCENT TO R.A.	0.

LOAD FACTOR MULTIPLIERS

LIGHTS	0.80
APPLIANCES	0.50
PEOPLE	0.80
PUMP HEAT	1.00

AIR QUANTITY FACTORS

JOB SITE ALTITUDE	0 FT
BAROMETRIC PRESSURE	29.921
AIR DENSITY FACTOR	1.000

VENTILATION

CEV/SF	0.50
CEV/PERSON	10.00
AIR CHANGE/HR	2.60
PCT. FAN CEV	0.00

INFILTRATION

AIR CHANGE/HR	0.00
DIVERSITY FACTOR	0.80

1 2 3 4 5 6 7 8
RUN OPTIONS USED 0 0 1 0 0 1 0 1

AUTOMATED PROCEDURES FOR ENGINEERING CONSULTANTS, ILC.

HVAC CALCULATION, HCC-111(42) CAPACITE-MARTIN AND ASS. SAN JUAN, P.R.

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BUILDING LOADS SUMMARY

	HEAT GAIN - COOLING		HEAT LOSS	
	SENSIBLE	LATENT	HEATING	WINTER GAIN
WINDOW TRANS	14704.		0.	
WINDOW SOLAR	15416.			0.
WALL	47218.		0.	
ROOF/CEILING	2252.		0.	
PARTITION	0.		0.	
FLOOR	0.		0.	
DOOR	0.		0.	
INFILTRATION	0.	0.	0.	
LIGHTS	267076.			267076.
PEOPLE (311)	8423.	8423.		8423.
APPLIANCES	87000.	0.		87000.
TOTALS	441891.	8423.	0.	362490.
TOTAL HEAT	450314.		PLMV HT 0.	
AT PEAK HOUR	15		VENT. 309452.	
SENS. HEAT RATIO	0.94		TOTAL HUMID 377520.	31.0 BTUH/SF
LIGHT HEAT TO R.A.		0.		
SKYLIGHT HEAT TO R.A.		0.	686972.	HEATING+HUMID
VENTILATION CFM	13000.		-53047.	LOSS LFSS INT. GAIN
EXHAUST CFM	0.		-53047.	LOSS LFSS INT.+SOLAR
PUMP HEAT FACTOR		1.00		
BUILDING REFRIGERATION LOAD		1059002.		
TONS OF REFRIGERATION		PR		

REFERENCE VALUES

	AREA	VOLUME	BTUH/SF		BTUH/CF		SF PER		CFM/SF
			COOL	HEAT	COOL	HEAT	TON	MBH	
COOLING	9990.	267732.	106.0	0.0	4.0	0.0	113.5	0.0	2.7
HEATING	0.	0.	0.0	0.0	0.0	0.0	0.0	0.0	0.0
TOTAL BLDG	9990.	267732.	106.0	31.0	4.0	1.2	113.5	32.3	2.7

AUTOMATED PROCEDURES FOR ENGINEERING CONSULTANTS, INC.

HVAC-CALCULATION, HCC-III (02) CAPACITE-MARTIN AND ASS. SAN JUAN, PR.

PROJECT - 8495 CENTER FOR ENERGY & ENVIRONMENT RESEARCH 10/12/79 PAGE 1

BUILDING HOURLY COOLING LOADS (*-BLDG. REFG. INCLUDES VENTILATION)

HOUP SENSIBLE	8	9	10	11	12	13
WIN TRANS	5514.	0.	3676.	2190.	12866.	14704.
WIN SOLAR	40752.	52505.	55237.	52447.	46443.	37340.
WALL	14871.	13491.	13486.	13480.	13480.	17982.
ROOF/CEILING	2235.	2017.	1908.	1799.	1799.	1799.
FLOOR	0.	0.	0.	0.	0.	0.
DOOR	0.	0.	0.	0.	0.	0.
INFILT	0.	0.	0.	0.	0.	0.
LIGHT TO RM	267076.	267076.	267076.	267076.	227015.	267076.
PEOPLE	8423.	8423.	8423.	8423.	7159.	8423.
APPLIANCE	87000.	87000.	87000.	87000.	73949.	87000.
TOTAL (INCL. PARTITIONS)	414852.	430514.	426808.	430417.	392715.	434326.
LATENT INFILT	0.	0.	0.	0.	0.	0.
PEOPLE	8423.	8423.	8423.	8423.	7159.	8423.
APPLIANCE	0.	0.	0.	0.	0.	0.
TOTAL	8423.	8423.	8423.	8423.	7159.	8423.
TOTAL LOAD	423275.	438937.	445231.	447840.	389875.	442750.
BLDG REFG. *	829208	906203	930302	863191	844174	1042833
TONS	69	75	77	80	73	87
HOUP SENSIBLE	14	15	16	17	18	19
WIN TRANS	14704.	14704.	14704.	12866.	11020.	9190.
WIN SOLAR	26020.	15416.	9095.	6969.	1881.	0.
WALL	38952.	47218.	49227.	49908.	49680.	51675.
ROOF/CEILING	1799.	2052.	3433.	5078.	6389.	7499.
FLOOR	0.	0.	0.	0.	0.	0.
DOOR	0.	0.	0.	0.	0.	0.
INFILT	0.	0.	0.	0.	0.	0.
LIGHT TO RM	267076.	267076.	267076.	267076.	0.	0.
PEOPLE	8423.	8423.	8423.	8423.	0.	0.
APPLIANCE	87000.	87000.	87000.	87000.	0.	0.
TOTAL (INCL. PARTITIONS)	443976.	441891.	439961.	437322.	58980.	68355.
LATENT INFILT	0.	0.	0.	0.	0.	0.
PEOPLE	8423.	8423.	8423.	8423.	0.	0.
APPLIANCE	0.	0.	0.	0.	0.	0.
TOTAL	8423.	8423.	8423.	8423.	0.	0.
TOTAL LOAD	452400.	458314.	447384.	445745.	69080.	68355.
BLDG REFG. *	1056605.	1058002.	1012003.	977204.	908630.	861501.
TONS	83	98	84			

$\sum_{14}^8 = 726 \text{ TR. H.}$

C.E.E.R NW-3

AUTOMATED PROCEDURES FOR ENGINEERING CONSULTANTS, INC.

MAG CALCULATION, HCC-III(G2) CARACETE-MARTIN AND ASS. SAN JUAN, PR.
 PROJECT - 8495 CENTER FOR ENERGY & ENVIRONMENT RESEARCH 10/12/78 PAGE 1

WEATHER PROFILES

HOURS	8	9	10	11	12	13	14	15	16	17	18	19	
MONTH 1	71.	72.	76.	80.	82.	83.	83.	83.	83.	82.	81.	80.	DR
	67.8	69.7	71.1	72.0	74.5	74.6	74.2	73.6	73.4	72.9	73.2	72.9	DR
	139	140	153	159	167	166	162	157	155	154	159	167	HR X 10000
MONTH 3	77.	79.	81.	83.	84.	84.	84.	84.	83.	82.	81.	80.	DR
	73.3	74.6	74.2	74.3	74.1	75.1	74.6	74.2	73.6	72.9	72.4	72.6	WH
	169	175	167	163	159	168	163	160	157	154	152	156	HR X 10000

GEOGRAPHIC/SOLAR DATA

LATITUDE	18.44
GROUND REFLECTIVITY	0.20
CLEARNESS FACTOR	1.00
MAX. SOLAR GAIN, BTUH/SF	90.00
DEGS. FROM STD. MERIDIAN	-5.00

INWARD FLOW FRACTIONS

NI	MIU	NIR
0.33	0.00	0.00
DAYLIGHT SVG. J F M A M J J A S O N D		
IN EFFECT 0 0 0 0 0 0 0 0 0 0 0 0		

DESIGN CONDITIONS

	WINTER	SUMMER
INSIDE		
TEMPERATURE	74.0	76.0
RELATIVE HUM	50.0	55.0
HUMIDITY RAT	0.0096	0.0106
OUTSIDE		
TEMPERATURE, DR	0.0	84.0
TEMPERATURE, WR	0.0	75.1
MONTH	1	3

MASTER BUILDING DATA

BLDG. ORIENT.	65.0 DEG.	CORR. FACT.
WALL HEIGHT	26.80 FEET	
HOOR AVERAGE	5	
COOLING D.T.	20.0 DEG.	
HEATING D.T.	50.0 DEG.	
HEATING LOAD	NO	
COOLING LOAD	YES	
OMIT WINT. SUN	NO	
CIRC. RATE	0.00 AC/HP, MIN	
COIL R.P. FAC.	0.10	
R.A. PLENUMS	NO	
CALC. APP.	NO	

OCCUPANCY

RTU/PERSON, SENS.	255.
RTU/PERSON, LAT.	255.
LOAD PROFILE NO.	1
SE/PERSON	0.00
MAX. NO. OF PEOPLE	40

LIGHTING

WATTS/SF	9.80
LOAD PROFILE NO.	2
PERCENT TO R.A.	0.

LOAD FACTOR MULTIPLIERS

LIGHTS	0.80
APPLIANCES	0.50
PEOPLE	0.80
PUMP HEAT	1.00

AIR QUANTITY FACTORS

JOB SITE ALTITUDE	0 FT
BAROMETRIC PRESSURE	29.921
AIR DENSITY FACTOR	1.000

VENTILATION

CFM/SF	0.50
CFM/PERSON	10.00
AIR CHANGE/HR	2.60
PCT. MAX. CFM	0.00

INFILTRATION

AIR CHANGE/HR	0.00
DIVERSITY FACTOR	0.80

1 2 3 4 5 6 7 8
 RUN OPTIONS USED 0 0 1 0 0 1 0 1

AUTOMATED PROCEDURES FOR ENGINEERING CONSULTANTS, INC.

HVAC CALCULATION, HCC-III(02) CAPACITE-MARTIN AND ASS. SAN JUAN, P.R.
PROJECT - 8496 CENTER FOR ENERGY & ENVIRONMENT RESEARCH 10/12/78 PAGE 12

BUILDING LOADS SUMMARY

Table with columns: HEAT GAIN - COOLING (SENSIBLE, LATENT), HEAT LOSS (HEATING, WINTER GAIN), and other load components like WINDOW TRANS, WINDOW SOLAR, WALL, ROOF/CEILING, PARTITION, FLOOR, DOOR, INFILTRATION, LIGHTS, PEOPLE, APPLIANCES, TOTALS, TOTAL HEAT AT PEAK HOUR, SENS. HEAT RATIO, LIGHT HEAT TO R.A., SKYLIGHT HEAT TO R.A., VENTILATION CFM, EXHAUST CFM, PUMP HEAT FACTOR, BUILDING REFRIGERATION LOAD, TONS OF REFRIGERATION.

REFERENCE VALUES table with columns: AREA, VOLUME, RTUH/SF (COOL, HEAT), RTUH/CF (COOL, HEAT), SF PER TON, CFM/SF (COOL), and rows for COOLING, HEATING, TOTAL BLDG.

AUTOMATED PROCEDURES FOR ENGINEERING CONSULTANTS, INC.

HVAC CALCULATION, HCC-111(02) CAPACITE-MARTIN AND ASS. SAN JUAN, PR.

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BUILDING HOURLY COOLING LOADS (*-BLDG. REFG. INCLUDES VENTILATION)

HR	8	9	10	11	12	13
SENSIBLE						
WIN TRANS	1939.	5514.	9190.	12866.	14704.	14704.
WIN SOLAR	36224.	43804.	44709.	40558.	33367.	24517.
WALL	21474.	20099.	20099.	21464.	22834.	34900.
ROOF/CEILING	3372.	3263.	3263.	3154.	3154.	3263.
FLOOR	0.	0.	0.	0.	0.	0.
DOOR	0.	0.	0.	0.	0.	0.
INFILT	0.	0.	0.	0.	0.	0.
LIGHT TO RM	267076.	267076.	267076.	267076.	227015.	267076.
PEOPLE	8423.	8423.	8423.	8423.	7159.	8423.
APPLIANCE	87000.	87000.	87000.	87000.	73949.	87000.
TOTAL (INCL. PARTITIONS)	425409.	435191.	439761.	440543.	382185.	430996.

LATENT						
INFILT	0.	0.	0.	0.	0.	0.
PEOPLE	8423.	8423.	8423.	8423.	7159.	8423.
APPLIANCE	0.	0.	0.	0.	0.	0.
TOTAL	8423.	8423.	8423.	8423.	7159.	8423.

TOTAL LOAD	433832.	442604.	449195.	448966.	399344.	448309.
BLDG REFG. *	29557.	101245.	100514.	101825.	93085.	106098.
TONS	77	84	84	85	77	93

HR	14	15	16	17	18	19
SENSIBLE						
WIN TRANS	14704.	14704.	12866.	11028.	9190.	7352.
WIN SOLAR	16353.	12750.	13222.	13602.	6166.	0.
WALL	49680.	54928.	56313.	55260.	51091.	52467.
ROOF/CEILING	3372.	3879.	5499.	7016.	8295.	9258.
FLOOR	0.	0.	0.	0.	0.	0.
DOOR	0.	0.	0.	0.	0.	0.
INFILT	0.	0.	0.	0.	0.	0.
LIGHT TO RM	267076.	267076.	267076.	267076.	0.	0.
PEOPLE	8423.	8423.	8423.	8423.	0.	0.
APPLIANCE	87000.	87000.	87000.	87000.	0.	0.
TOTAL (INCL. PARTITIONS)	446620.	449763.	450401.	449408.	75643.	69077.

LATENT						
INFILT	0.	0.	0.	0.	0.	0.
PEOPLE	8423.	8423.	8423.	8423.	0.	0.
APPLIANCE	0.	0.	0.	0.	0.	0.
TOTAL	8423.	8423.	8423.	8423.	0.	0.

TOTAL LOAD	455043.	457196.	459924.	457031.	75643.	69077.
BLDG REFG. *	104334.	103022.	95006.	96619.	36400.	33463.
TONS	87	86	83			

$\sum_{19}^4 = 751 \text{ T.L.H}$

AUTOMATED PROCEDURES FOR ENGINEERING CONSULTANTS, INC.

HVIC CALCULATION, MCC-BH(102) CAPACITE-MARTIN AND ASS. SAN JUAN, PR.

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WEATHER PROFILES

HOURS	8	9	10	11	12	13	14	15	16	17	18	19
MONTH 1	71.8	73.7	74.8	80.0	82.0	83.0	83.0	83.0	82.0	81.0	80.0	DR
	67.8	69.7	71.1	73.0	74.5	74.6	74.2	73.6	73.4	72.9	73.2	72.8
	130	140	153	150	167	166	162	167	156	154	150	157
												HR X 1000
MONTH 4	73.0	75.0	77.0	79.0	82.0	84.0	84.0	84.0	84.0	83.0	82.0	DR
	70.2	70.8	71.6	72.7	74.0	75.0	75.1	75.9	75.7	76.0	75.6	75.4
	153	153	155	161	171	174	177	175	173	176	175	175
												HR X 1000

GEOGRAPHIC/SOLAR DATA

LATITUDE	18.44
GROUND REFLECTIVITY	0.20
CLEARNESS FACTOR	1.00
MAX. SOLAR GAIN, BTU/HR/FT ²	80.00
DEGS. FROM STD. MERIDIAN	-5.00

INWARD FLOW FRACTIONS

NI	NIU	NIR
0.33	0.00	0.00
DAYLIGHT SVG. J F M A M J J A S O N D		
IN EFFECT 0 0 0 0 0 0 0 0 0 0 0 0		

DESIGN CONDITIONS

	WINTER	SUMMER
INSIDE		
TEMPERATURE	74.0	76.0
RELATIVE HUM	50.0	55.0
HUMIDITY RAT	0.0096	0.0106
OUTSIDE		
TEMPERATURE, DR	0.0	84.0
TEMPERATURE, WR	0.0	76.1
MONTH	1	4

MASTER BUILDING DATA

BLOG. ORIENT.	65.0 DEG. CORR. FACT.
WALL HEIGHT	26.00 FEET
HOOR AVERAGE	5
COOLING D.T.	20.0 DEG.
HEATING D.T.	50.0 DEG.
HEATING LOAD	NO
COOLING LOAD	YES
OMIT WINT. SUN	NO
CIRC. RATE	0.00 AC/HR, MIN
COIL R.P. FAC.	0.10
R.A. PLENUMS	NO
CALC. ADP	NO

OCCUPANCY

RTU/PERSON, SENS.	255.
RTU/PERSON, LAT.	255.
LOAD PROFILE NO.	1
SE/PERSON	0.00
MAX. NO. OF PEOPLE	40

LIGHTING

WATTS/SE	9.80
LOAD PROFILE NO.	2
PERCENT TO R.A.	0.

LOAD FACTOR MULTIPLIERS

LIGHTS	0.80
APPLIANCES	0.50
PEOPLE	0.80
DIVID. HEAT	1.00

AIR QUANTITY FACTORS

JOB SITE ALTITUDE	0 FT
BARYMETRIC PRESSURE	29.921
AIR DENSITY FACTOR	1.000

VENTILATION

CFM/SE	0.50
CFM/PERSON	10.00
AIR CHANGE/HR	2.60
PCT. FAN CFM	0.00

INFILTRATION

AIR CHANGE/HR	0.00
DIVERSITY FACTOR	0.80

1 2 3 4 5 6 7 8
RUN OPTIONS USED 0 0 1 0 0 1 0 1

AUTOMATED PROCEDURES FOR ENGINEERING CONSULTANTS, INC.

HVAC CALCULATION, HCC-III(02) - CAPACITE-MARTIN AND ASS. SAN JUAN, PR.

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BUILDING LOADS SUMMARY

	HEAT GAIN - COOLING		HEAT LOSS	
	SENSIBLE	LATENT	HEATING	WINTER GAIN
WINDOW TRANS.	14784.		0.	
WINDOW SOLAR	21310.			0.
WALL	47140.		0.	
ROOF/CEILING	7306.		0.	
PARTITION	0.		0.	
FLOOR	0.		0.	
DOOR	0.		0.	
INFILTRATION	0.	0.	0.	
LIGHTS	267076.			267076.
PEOPLE (31)	8423.	8423.		8423.
APPLIANCES	87000.	0.		87000.
TOTALS	452962.	8423.	0.	362499.
TOTAL HEAT AT PEAK HOUR	461385.		PLNM HT VENT. 252823.	
SENS. HEAT RATIO	0.9		TOTAL HUMID 281424.	25.3 BTUH/SF
LIGHT HEAT TO R.A.	0.			
SKYLIGHT HEAT TO R.A.	0.		534248.	HEATING+HUMID
VENTILATION CFM	13000.		-109675.	LOSS LESS INT. GAIN
EXHAUST CFM	0.		-109675.	LOSS LESS INT.+SOLAR
PUMP HEAT FACTOR		1.00		
BUILDING REFRIGERATION LOAD		1121846.		
TONS OF REFRIGERATION		93.		

REFERENCE VALUES

	AREA	VOLUME	BTUH/SF		BTUH/CF		SF PER		CFM/SF COOL
			COOL	HEAT	COOL	HEAT	TON	MRH	
COOLING	9990.	267732.	112.3		4.2		107.4		2.8
HEATING	0.	0.		0.0		0.0		0.0	
TOTAL BLDG	9990.	267732.	112.3	25.3	4.2	0.9	107.4	39.5	2.8

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AUTOMATED PROCEDURES FOR ENGINEERING CONSULTANTS, INC.

HVAC CALCULATION, MCC-III(02) CAPACITE-MARTIN AND ASS. SA: JUAN, PR.

PROJECT - 5495 CENTER FOR ENERGY & ENVIRONMENT RESEARCH 10/12/78 PAGE 11

BUILDING HOURLY COOLING LOADS (*-PLDG. REFG. INCLUDES VENTILATION)

W. O. P.	8	9	10	11	12	13
SENSIBLE						
WIN TRANS	5514.	1038.	1038.	3676.	11028.	14704.
WIN SOLAR	26610.	31197.	30825.	26475.	20691.	15713.
WALL	25101.	23725.	23720.	22345.	22345.	38926.
ROOF/CEILING	4122.	4018.	3904.	3705.	3795.	3686.
FLOOR	0.	0.	0.	0.	0.	0.
DOOR	0.	0.	0.	0.	0.	0.
INFILT	0.	0.	0.	0.	0.	0.
LIGHT TO RM	267076.	267076.	267076.	267076.	227015.	267076.
PEOPLE	8423.	8423.	8423.	8423.	7159.	8423.
APPLIANCE	87000.	87000.	87000.	87000.	73949.	87000.
TOTAL (INCL. PARTITIONS)	412819.	419598.	422799.	418792.	365985.	434531.

LATENT						
INFILT	0.	0.	0.	0.	0.	0.
PEOPLE	8423.	8423.	8423.	8423.	7159.	8423.
APPLIANCE	0.	0.	0.	0.	0.	0.
TOTAL	8423.	8423.	8423.	8423.	7159.	8423.

TOTAL LOAD	421242.	428021.	431211.	427215.	373144.	442854.
BLDG REFG. *	776224.	807619.	850351.	896572.	932617.	1084151.
TONS	65	67	71	74	77	90
HOUR	14	15	16	17	18	19

W. O. P.	14	15	16	17	18	19
SENSIBLE						
WIN TRANS	14704.	14704.	14704.	14704.	12866.	11028.
WIN SOLAR	16572.	19003.	21780.	21310.	10671.	0.
WALL	44315.	48508.	49566.	47140.	47541.	48873.
ROOF/CEILING	3686.	4541.	5885.	7306.	8489.	9257.
FLOOR	0.	0.	0.	0.	0.	0.
DOOR	0.	0.	0.	0.	0.	0.
INFILT	0.	0.	0.	0.	0.	0.
LIGHT TO RM	267076.	267076.	267076.	267076.	0.	0.
PEOPLE	8423.	8423.	8423.	8423.	0.	0.
APPLIANCE	87000.	87000.	87000.	87000.	0.	0.
TOTAL (INCL. PARTITIONS)	441778.	449258.	454437.	452962.	79569.	70159.

LATENT						
INFILT	0.	0.	0.	0.	0.	0.
PEOPLE	8423.	8423.	8423.	8423.	0.	0.
APPLIANCE	0.	0.	0.	0.	0.	0.
TOTAL	8423.	8423.	8423.	8423.	0.	0.

TOTAL LOAD	450201.	457681.	462261.	461385.	79569.	70159.
BLDG REFG. *	1110773.	1111047.	1107707.	1121446.	480142.	437561.
TONS	93	93	95			

$\sum_{14}^8 = 723 \text{ TON. H}$

AUTOMATED PROCEDURES FOR ENGINEERING CONSULTANTS, INC.

HVAC CALCULATION, HCC-III(02) CAPACITE-MARTIN AND ASS. SAN JUAN, PR.

PROJECT - 8495 CENTER FOR ENERGY & ENVIRONMENT RESEARCH 10/12/78 PAGE

WEATHER PROFILES

HOURS	9	10	11	12	13	14	15	16	17	18	19	
MONTH 1	71.	73.	76.	80.	82.	83.	82.	82.	82.	81.	80.	DB
	67.8	69.7	71.1	73.0	74.5	74.6	74.2	73.6	73.4	72.9	72.2	WB
	120	140	153	159	167	166	162	157	156	154	152	HR X 1000
MONTH 5	75.	77.	79.	82.	84.	86.	87.	87.	87.	86.	85.	DB
	70.9	71.0	71.0	72.3	73.9	75.4	76.3	76.3	76.7	77.1	76.7	WB
	154	150	145	140	157	166	171	171	175	179	178	HR X 1000

GEOGRAPHIC/SOLAR DATA

INWARD FLOW FRACTIONS

LATITUDE	18.44	NI	NIU	NIR
GROUND REFLECTIVITY	0.20	0.33	0.00	0.00
CLEARNESS FACTOR	1.00			
MAX. SOLAR GAIN, BTU/SE	80.00	DAYLIGHT SVC.	J F M A M J J A S O N D	
DEGS. FROM STD. MERIDIAN	-5.00	IN EFFECT	0 0 0 0 0 0 0 0 0 0 0 0	

DESIGN CONDITIONS

MASTER BUILDING DATA

	WINTER	SUMMER	
INSIDE			BLDG. ORIENT. 65.0 DEG. CORR. FACT.
TEMPERATURE	74.0	76.0	WALL HEIGHT 26.80 FEET
RELATIVE HUM	50.0	55.0	HOUR AVERAGE 5
HUMIDITY RAT	0.0096	0.0106	COOLING D.T. 20.0 DEG.
OUTSIDE			HEATING D.T. 50.0 DEG.
TEMPERATURE, DB	0.0	87.0	HEATING LOAD NO
TEMPERATURE, WB	0.0	77.1	COOLING LOAD YES
MONTH	1	5	OMIT WINT. SUN NO
			CIRCN. RATE 0.00 AC/HP, MIN
			COIL R.P. FAC. 0.10
			R.A. PLENUMS NO
			CALC. ADP NO

OCCUPANCY

LIGHTING

RTU/PERSON, SEAS.	255.	WATTS/SE	9.80
RTU/PERSON, LAT.	255.	LOAD PROFILE NO.	2
LOAD PROFILE NO.	1	PERCENT TO R.A.	0.
SE/PERSON	0.00		
MAX. NO. OF PEOPLE	40		

LOAD FACTOR MULTIPLIERS

AIR QUANTITY FACTORS

LIGHTS	0.80	JOB SITE ALTITUDE	0 FT
APPLIANCES	0.50	BAROMETRIC PRESSURE	29.921
PEOPLE	0.80	AIR DENSITY FACTOR	1.000
PUMP HEAT	1.00		

VENTILATION

INFILTRATION

CFM/SE	0.50	AIR CHANGE/HR	0.00
CFM/PERSON	10.00	DIVERSITY FACTOR	0.80
AIR CHANGE/HR	2.60		
PCT. FAN CFM	0.00		

1 2 3 4 5 6 7 8
 RUN OPTIONS USED 0 0 1 0 0 1 0 1

AUTOMATED PROCEDURES FOR ENGINEERING CONSULTANTS, INC.

HVAC CALCULATION, HCC-III(02) - CAPACITE-MARTIN AND ASS. SAN JUAN, PR.

PROJECT - 8495 CENTER FOR ENERGY & ENVIRONMENT RESEARCH 10/12/78 PAGE 1

BUILDING LOADS SUMMARY

	HEAT GAIN - COOLING		HEAT LOSS	
	SENSIBLE	LATENT	HEATING	WINTER GAIN
WINDOW TRANS	20210.		0.	
WINDOW SOLAR	26070.			0.
WALL	58058.		0.	
ROOF CEILING	8617.		0.	
PARTITION	0.		0.	
FLOOR	0.		0.	
DOOR	0.		0.	
INFILTRATION	0.	0.	0.	
LIGHTS	267076.			267076.
PEOPLE (- 31)	8423.	8423.		8423.
APPLIANCES	87000.	0.		87000.
TOTALS	475465.	8423.	0.	352499.
TOTAL HEAT	483890.		PLNM HT. VENT. 0.	
AT PEAK HOUR	17		287716.	
SENS. HEAT RATIO	0.99		TOTAL HUMID 291147.	28.8 BTUH/SF
LIGHT HEAT TO P.A.		0.		
SKYLIGHT HEAT TO P.A.		0.	578864.	HEATING+HUMID
VENTILATION CFM	13000.		-74783.	LOSS LESS INT. GAIN
EXHAUST CFM	0.		-74783.	LOSS LESS INT.+SOLAR
PUMP HEAT FACTOR		1.00		
BUILDING REFRIGERATION LOAD		1216750.		
TONS OF REFRIGERATION		101		

REFERENCE VALUES

	AREA	VOLUME	BTUH/SF		BTUH/CF		SF PER		CFM/SF COOL
			COOL	HEAT	COOL	HEAT	TON	MHH	
COOLING	9990.	267732.	121.8		4.5		98.9		2.9
HEATING	0.	0.		0.0		0.0		0.0	
TOTAL BLDG	9990.	267732.	121.8	28.8	4.5	1.1	98.9	34.7	2.9

AUTOMATED PROCEDURES FOR ENGINEERING CONSULTANTS, INC.

MAC-CALCULATION, HCC-11102) - CAPACETE-MARTIN AND ASS. SAN JUAN, PR.
 PROJECT - CASE CENTER FOR ENERGY & ENVIRONMENT RESEARCH 10/12/78 PAGE 1

BUILDING HOURLY COOLING LOADS (*-BLDG. REFG. INCLUDES VENTILATION)

HR	8	9	10	11	12	13
SENSIBLE						
WIN TRANS	1839.	1839.	5514.	11028.	14704.	12381.
WIN SOLAR	19868.	23035.	22731.	20040.	17754.	12667.
WALL	32202.	31827.	30452.	30447.	30789.	45787.
ROOF/CEILING	5221.	5112.	5003.	4894.	4784.	4784.
FLOOR	0.	0.	0.	0.	0.	0.
DOOR	0.	0.	0.	0.	0.	0.
INFILT	0.	0.	0.	0.	0.	0.
LIGHT TO RM	267076.	267076.	267076.	267076.	227015.	267076.
PEOPLE	8423.	8423.	8423.	8423.	7159.	8423.
APPLIANCE	87000.	87000.	87000.	87000.	73949.	87000.
TOTAL (INCL. PARTITIONS)	418954.	424313.	426201.	428010.	375158.	450040.
LATENT						
INFILT	0.	0.	0.	0.	0.	0.
PEOPLE	8423.	8423.	8423.	8423.	7159.	8423.
APPLIANCE	0.	0.	0.	0.	0.	0.
TOTAL	8423.	8423.	8423.	8423.	7159.	8423.
TOTAL LOAD BLDG REFG. *	427377.	432737.	424624.	427333.	383317.	459463.
	810033.	825369.	836132.	809876.	810526.	1094124.
TONS	67	69	70	76	75	42
HR	14	15	16	17	18	19
SENSIBLE						
WIN TRANS	20219.	20219.	20219.	20219.	18381.	16542.
WIN SOLAR	21608.	25471.	27757.	26070.	14472.	0.
WALL	52713.	56484.	57531.	58058.	56023.	60587.
ROOF/CEILING	4796.	5005.	7281.	8617.	9724.	13650.
FLOOR	0.	0.	0.	0.	0.	0.
DOOR	0.	0.	0.	0.	0.	0.
INFILT	0.	0.	0.	0.	0.	0.
LIGHT TO RM	267076.	267076.	267076.	267076.	0.	0.
PEOPLE	8423.	8423.	8423.	8423.	0.	0.
APPLIANCE	87000.	87000.	87000.	87000.	0.	0.
TOTAL (INCL. PARTITIONS)	441836.	470590.	475280.	475465.	98601.	87790.
LATENT						
INFILT	0.	0.	0.	0.	0.	0.
PEOPLE	8423.	8423.	8423.	8423.	0.	0.
APPLIANCE	0.	0.	0.	0.	0.	0.
TOTAL	8423.	8423.	8423.	8423.	0.	0.
TOTAL LOAD BLDG REFG. *	470250.	470003.	483712.	483890.	98601.	87790.
	1152272.	1144024.	1194582.	1216750.	592787.	547350.
TONS	96	97	99			

$\sum_{14}^8 = 711 \text{ TONS H}$

AUTOMATED PROCEDURES FOR ENGINEERING CONSULTANTS, INC.

HVAC CALCULATION, HCC-III(02) - CAPACETH-MARTIN AND ASS. SAN JUAN, P.R.

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WEATHER PROFILES

HOURS	8	9	10	11	12	13	14	15	16	17	18	19
MONTH 1	71.0	72.0	76.0	80.0	82.0	82.0	83.0	82.0	82.0	82.0	81.0	80.0
	57.8	60.7	71.1	73.0	74.5	74.6	74.2	73.6	73.4	72.9	73.2	72.8
	130	140	153	159	167	156	152	157	156	154	159	157
												HR X 1000
MONTH 6	78.0	80.0	83.0	85.0	87.0	88.0	89.0	87.0	87.0	86.0	85.0	84.0
	74.2	75.1	76.1	77.2	78.8	79.0	78.7	78.0	78.2	78.0	77.3	77.2
	174	177	179	184	195	194	192	187	189	190	185	187
												HR X 1000

GEOGRAPHIC/SOLAR DATA

LATITUDE	18.44
GROUND REFLECTIVITY	0.20
CLEARNESS FACTOR	1.00
MAX. SOLAR GAIN, BTUH/SF	80.00
DEGS. FROM STD. MERIDIAN	-5.00

INWARD FLOW FRACTIONS

NI	MIU	MIR
0.93	0.00	0.00
DAYLIGHT SVG. J F M A M J J A S O N D		
IN EFFECT 0 0 0 0 0 0 0 0 0 0 0		

DESIGN CONDITIONS

	WINTER	SUMMER
INSIDE		
TEMPERATURE	76.0	76.0
RELATIVE HUM	50.0	55.0
HUMIDITY RAT	0.0096	0.0106
OUTSIDE		
TEMPERATURE, DR	0.0	88.0
TEMPERATURE, WR	0.0	79.0
MONTH	1	6

MASTER BUILDING DATA

BLDG. ORIENT.	65.0 DEG.	COOR. FACT.
WALL HEIGHT	26.80 FEET	
HOOR AVERAGE	5	
COOLING D.T.	20.0 DEG.	
HEATING D.T.	50.0 DEG.	
HEATING LOAD	NO	
COOLING LOAD	YES	
OMIT WINT. SUN	NO	
CIRC. RATE	0.00 AC/HR, MIN	
COIL R.P. FAC.	0.10	
R.A. PLENUMS	NO	
CALC. - ADP	NO	

OCCUPANCY

BTU/PERSON, SENS.	255
BTU/PERSON, LAT.	255
LOAD PROFILE NO.	1
SE/PERSON	0.00
MAX. NO. OF PEOPLE	40

LIGHTING

WATTS/SF	9.80
LOAD PROFILE NO.	2
PERCENT TO R.A.	0.

LOAD FACTOR MULTIPLIERS

LIGHTS	0.80
APPLIANCES	0.50
PEOPLE	0.80
PUMP HEAT	1.00

AIR QUANTITY FACTORS

JCR SITE ALTITUDE	0 FT
BAROMETRIC PRESSURE	29.921
AIR DENSITY FACTOR	1.000

VENTILATION

CFM/SF	0.50
CFM/PERSON	10.00
AIR CHANGE/HR	2.60
PCT. FAN CFM	0.00

INFILTRATION

AIR CHANGE/HR	0.00
DIVERSITY FACTOR	0.80

1 2 3 4 5 6 7 8
 RUN OPTIONS USED 0 0 1 0 0 1 0 1

AUTOMATED PROCEDURES FOR ENGINEERING CONSULTANTS, INC.

HVAC CALCULATION, HCC-III(92) - CAPACITE-MARTIN AND ASS. SAN JOAQUIN, CA.

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BUILDING LOADS SUMMARY

	HEAT GAIN - COOLING		HEAT LOSS	
	SENSIBLE	LATENT	HEATING	WINTER GAIN
WINDOW TRANS	22057.		0.	
WINDOW SOLAR	22719.			0.
WALL	59071.		0.	
ROOF/CEILING	5292.		0.	
PARTITION	0.		0.	
FLOOR	0.		0.	
DOOR	0.		0.	
INFILTRATION	0.	0.	0.	
LIGHTS	267076.			267076.
PEOPLE (31)	8423.	8423.		8423.
APPLIANCES	87000.	0.		87000.
TOTALS	472640.	8423.	0.	262499.
TOTAL HEAT	481063.		PLMW HT	0.
AT PEAK HOUR	14		VENT.	456455.
SENS. HEAT RATIO	0.99		TOTAL HUMID	456455.
LIGHT HEAT TO P.A.		0.		45.7 BTUH/SF
SKYLIGHT HEAT TO P.A.		0.	960387.	HEATING+HUMID
VENTILATION CFM	13000.		93956.	LOSS LESS INT. GAIN
EXHAUST CFM	0.		93956.	LOSS LESS INT.+SOLAR
PUMP HEAT FACTOR		1.00		
BUILDING REFRIGERATION LOAD		1298632.		
TONS OF REFRIGERATION		108.		

REFERENCE VALUES

	AREA	VOLUME	BTUH/SF		BTUH/CF		SF PER		CFM/SF COOL
			COOL	HEAT	COOL	HEAT	TON	MPH	
COOLING	9990.	267732.	130.0		4.9		92.5		2.9
HEATING	0.	0.		0.0		0.0		0.0	
TOTAL BLDG	9990.	267732.	130.0	45.7	4.9	1.7	92.5	21.9	2.9

AUTOMATED PROCEDURES FOR ENGINEERING CONSULTANTS, INC.

HVAC CALCULATION, HCC-III(02) - CAPACITE-MARTIN AND ASS. SAN JUAN, P.R.

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BUILDING HOURLY COOLING LOADS (*-BLDG. REFG. INCLUDES VENTILATION)

LOAD	8	9	10	11	12	13
SENSIBLE						
WIN TRANS	3674.	7352.	12866.	18842.	20219.	22357.
WIN SOLAR	17342.	20463.	20752.	19284.	18433.	20239.
WALL	37750.	26374.	26369.	24904.	35243.	50549.
ROOF/CEILING	5720.	5611.	5502.	5393.	5393.	5284.
FLOOR	0.	0.	0.	0.	0.	0.
DOOR	0.	0.	0.	0.	0.	0.
INFILT	0.	0.	0.	0.	0.	0.
LIGHT TO RM	267076.	267076.	267076.	267076.	227015.	267076.
PEOPLE	8423.	8423.	8423.	8423.	7159.	8423.
APPLIANCE	87000.	87000.	87000.	87000.	73949.	87000.
TOTAL (INCL. PARTITIONS)	426989.	432301.	437991.	438714.	387413.	460630.
LATENT						
INFILT	0.	0.	0.	0.	0.	0.
PEOPLE	8423.	8423.	8423.	8423.	7159.	8423.
APPLIANCE	0.	0.	0.	0.	0.	0.
TOTAL	8423.	8423.	8423.	8423.	7159.	8423.
TOTAL LOAD	435412.	440724.	446414.	447137.	394573.	469053.
BLDG REFG. *	868836.	1027438.	1008645.	1159739.	1168429.	1295779.
TONS	81	86	92	97	98	108
HOUR	14	15	16	17	18	19
SENSIBLE						
WIN TRANS	22057.	20219.	20219.	18381.	16542.	14704.
WIN SOLAR	23719.	27602.	29756.	28150.	17962.	0.
WALL	59971.	63094.	65798.	65255.	64010.	66889.
ROOF/CEILING	5292.	6462.	7915.	9228.	10435.	11257.
FLOOR	0.	0.	0.	0.	0.	0.
DOOR	0.	0.	0.	0.	0.	0.
INFILT	0.	0.	0.	0.	0.	0.
LIGHT TO RM	267076.	267076.	267076.	267076.	0.	0.
PEOPLE	8423.	8423.	8423.	8423.	0.	0.
APPLIANCE	87000.	87000.	87000.	87000.	0.	0.
TOTAL (INCL. PARTITIONS)	472640.	479878.	486189.	483515.	109851.	92951.
LATENT						
INFILT	0.	0.	0.	0.	0.	0.
PEOPLE	8423.	8423.	8423.	8423.	0.	0.
APPLIANCE	0.	0.	0.	0.	0.	0.
TOTAL	8423.	8423.	8423.	8423.	0.	0.
TOTAL LOAD	481063.	488301.	494612.	491038.	109851.	92951.
BLDG REFG. *	1298532.	1265315.	1285471.	1270619.	513455.	566512.
TONS	108	107	107			

$\sum_{10}^8 = 234 TR. H$

AUTOMATED PROCEDURES FOR ENGINEERING CONSULTANTS, INC.

HVAC CALCULATION, HCC-III(02) CARACETE-MARTIN AND ASS. SAN JUAN, PR.

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WEATHER PROFILES

Table with columns for MONTH, HOURS, and temperature values (e.g., 71, 72, 76, 80, 82, 83, 83, 82, 81, 80, 80, 81, 83, 84, 85, 86, 86, 86, 85, 84, 84).

GEOGRAPHIC/SOLAR DATA

Table with columns for LATITUDE (18.44), GROUND REFLECTIVITY (0.20), CLEARNESS FACTOR (1.00), MAX. SOLAR GAIN, RTU/SE (80.00), DEGS. FROM STD. MERIDIAN (-5.00).

INWARD FLOW FRACTIONS

Table with columns for NI, IU, NIR, and DAYLIGHT SVG. (J F M A M J J A S O N D).

DESIGN CONDITIONS

Table with columns for WINTER and SUMMER, and rows for INSIDE TEMPERATURE, RELATIVE HUM, HUMIDITY RAT, OUTSIDE TEMPERATURE, DR, and MONTH.

MASTER BUILDING DATA

Table with rows for BLDG. ORIENT., WALL HEIGHT, HOUR AVERAGE, COOLING D.T., HEATING D.T., HEATING LOAD, COOLING LOAD, OMIT WINT. SUN, CIRCUL. RATE, COIL R.P. FAC., R.A. PLENUMS, and CALC. ADP.

OCCUPANCY

Table with rows for RTU/PERSON, GENL., RTU/PERSON, LAT., LOAD PROFILE NO., SE/PERSON, and MAX. NO. OF PEOPLE.

LIGHTING

Table with rows for WATTS/SE, LOAD PROFILE NO., and PERCENT TO R.A.

LOAD FACTOR MULTIPLIERS

Table with rows for LIGHTS, APPLIANCES, PEOPLE, and PLUMB HEAT.

AIR QUANTITY FACTORS

Table with rows for JOB SITE ALTITUDE, BAROMETRIC PRESSURE, and AIR DENSITY FACTOR.

VENTILATION

Table with rows for CFM/SE, CFM/PERSON, AIR CHANGE/HR, and PCT. FAN CFM.

INFILTRATION

Table with rows for AIR CHANGE/HR and DIVERSITY FACTOR.

1 2 3 4 5 6 7 8 RUN OPTIONS USED 0 0 1 0 0 1 0 1

AUTOMATED PROCEDURES FOR ENGINEERING CONSULTANTS, INC.

HVAC CALCULATION, HCC-III(02) CAPACITE-MARTIN AND ASS. SAN JOAQUIN, PP.

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BUILDING LOADS SUMMARY

	HEAT GAIN - COOLING		HEAT LOSS	
	SENSIBLE	LATENT	HEATING	WINTER GAIN
WINDOW TRANS	18381.		0.	
WINDOW SOLAR	25427.			0.
WALL	64086.		0.	
ROOF/CEILING	6360.		0.	
PARTITION	0.		0.	
FLOOR	0.		0.	
DOOR	0.		0.	
INFILTRATION	0.	0.	0.	
LIGHTS	267076.			267076.
PEOPLE (31)	8423.	8423.		8423.
APPLIANCES	87000.	0.		87000.
TOTALS	476754.	8423.	0.	362499.
TOTAL HEAT	485177.		PLNM HT	
AT PEAK HOUR	15		VENT.	573144.
SENS. HEAT RATIO	0.99		TOTAL	573144.
			HUMID	593736.
LIGHT HEAT TO R.A.		0.		
SKYLIGHT HEAT TO R.A.		0.	1166890.	HEATING+HUMID
VENTILATION CFM	13000.		210644.	LOSS LESS INT. GAIN
EXHAUST CFM	0.		210644.	LOSS LESS INT.+SOLAR
PUMP HEAT FACTOR		1.00		
BUILDING REFRIGERATION LOAD	1299257.			
TONS OF REFRIGERATION	108			

REFERENCE VALUES

	AREA	VOLUME	RTUH/SF		PTUH/CF		SF PER TON	CFY/SF
			COOL	HEAT	COOL	HEAT		
COOLING	9990.	267732.	130.1		4.9		92.5	2.9
HEATING	0.	0.		0.0		0.0		0.0
TOTAL BLDG	9990.	267732.	130.1	57.4	4.9	2.1	92.5	17.4

AUTOMATED PROCEDURES FOR ENGINEERING CONSULTANTS, INC.

MVAC CALCULATION, HCC-II (02) - CAPACITE-MARTIN AND ASS. SAN JUAN, PR.

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BUILDING HOURLY COOLING LOADS (*-BLDG. PEFG. INCLUDES VENTILATION)

HOUP	8	9	10	11	12	13
SENSIBLE						
WIN TRANS	7352.	9190.	12966.	14704.	19381.	19381.
WIN SOLAR	19612.	22427.	22772.	20599.	18314.	18939.
WALL	36863.	35493.	35488.	36953.	26853.	51970.
ROOF/CEILING	5461.	5461.	5352.	5243.	5243.	5352.
FLOOR	0.	0.	0.	0.	0.	0.
DOOR	0.	0.	0.	0.	0.	0.
INFILT	0.	0.	0.	0.	0.	0.
LIGHT TO RM	267076.	267076.	267076.	267076.	277015.	257076.
PEOPLE	8423.	8423.	8423.	8423.	7159.	8423.
APPLIANCE	87000.	87000.	87000.	87000.	73949.	87000.
TOTAL (INCL. PARTITIONS)	430789.	435073.	438979.	439900.	386917.	456542.
LATENT						
INFILT	0.	0.	0.	0.	0.	0.
PEOPLE	8423.	8423.	8423.	8423.	7159.	8423.
APPLIANCE	0.	0.	0.	0.	0.	0.
TOTAL	8423.	8423.	8423.	8423.	7159.	8423.
TOTAL LOAD	439213.	443496.	447403.	448323.	394076.	464956.
BLDG PEFG. *	1090255.	1110111.	1146550.	1175648.	1148541.	1278140.
TONS	90	92	95	98	46	106
HOUP	14	15	16	17	18	19
SENSIBLE						
WIN TRANS	18381.	18381.	18381.	16542.	14704.	14704.
WIN SOLAR	21612.	25427.	27901.	26799.	17383.	0.
WALL	60998.	64986.	65628.	63798.	62058.	62586.
ROOF/CEILING	5352.	6360.	7841.	9079.	10211.	10958.
FLOOR	0.	0.	0.	0.	0.	0.
DOOR	0.	0.	0.	0.	0.	0.
INFILT	0.	0.	0.	0.	0.	0.
LIGHT TO RM	267076.	267076.	267076.	267076.	0.	0.
PEOPLE	8423.	8423.	8423.	8423.	0.	0.
APPLIANCE	87000.	87000.	87000.	87000.	0.	0.
TOTAL (INCL. PARTITIONS)	468844.	476754.	482251.	478719.	104357.	82249.
LATENT						
INFILT	0.	0.	0.	0.	0.	0.
PEOPLE	8423.	8423.	8423.	8423.	0.	0.
APPLIANCE	0.	0.	0.	0.	0.	0.
TOTAL	8423.	8423.	8423.	8423.	0.	0.
TOTAL LOAD	477267.	485177.	490674.	487147.	104357.	82249.
BLDG PEFG. *	1287578.	1299257.	1296903.	1253307.	594453.	565964.
TONS	108	108	103			

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AUTOMATED PROCEDURES FOR ENGINEERING CONSULTANTS, I.C.

HVAC CALCULATION, HCC-III(02) - CAPACITE-MARTIN AND ASS. SAN JUAN, P.R.

PROJECT - 8485 CENTER FOR ENERGY & ENVIRONMENT RESEARCH 10/12/78 PAGE 1

WEATHER PROFILES

MO. YR.	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	
MONTH 1	71.	73.	76.	80.	82.	83.	83.	82.	82.	82.	81.	80.	80.	80.	82.	82.	82.	81.	80.	80.
	67.8	69.7	71.1	73.0	74.5	74.6	74.2	72.6	72.4	72.9	73.2	72.8	72.8	72.6	72.4	72.4	72.9	73.2	72.8	72.8
	130	140	153	160	167	166	162	157	156	154	159	157	157	157	156	154	159	157	157	157
MONTH 2	78.	80.	82.	83.	85.	86.	87.	87.	87.	87.	86.	85.	85.	85.	87.	87.	87.	86.	85.	85.
	75.9	76.0	76.3	76.6	77.7	79.0	79.0	79.5	79.5	79.3	79.2	79.2	79.2	79.2	79.5	79.5	79.3	79.2	79.2	79.2
	188	185	183	184	189	190	197	202	202	200	201	203	203	202	202	200	201	203	203	203

GEOGRAPHIC/SOLAR DATA

LATITUDE	18.44
GROUND REFLECTIVITY	0.20
CLEARNESS FACTOR	1.00
MAX. SOLAR GAIN, BTU/H/SF	80.00
DEGS. FROM STD. MERIDIAN	-5.00

INWARD FLOW FRACTIONS

NI	NIU	AIR
0.33	0.00	0.00
DAYLIGHT SVG. J F M A M J J A S O N D		
IN EFFECT 0 0 0 0 0 0 0 0 0 0 0 0		

DESIGN CONDITIONS

	WINTER	SUMMER
INSIDE		
TEMPERATURE	76.0	76.0
RELATIVE HUM	50.0	55.0
HUMIDITY RAT	0.0086	0.0106
OUTSIDE		
TEMPERATURE, DR	0.0	87.0
TEMPERATURE, WR	0.0	79.5
MONTH	1	2

MASTER BUILDING DATA

BLDG. ORIENT.	65.0 DEG.	CORR. FACT.
WALL HEIGHT	26.80 FEET	
HOUR AVERAGE	5	
COOLING D.T.	20.0 DEG.	
HEATING D.T.	50.0 DEG.	
HEATING LOAD	NO	
COOLING LOAD	YES	
ONIT WINT. SUN	NO	
CIPEN. RATE	0.00 AC/HR, MIN	
COIL R.P. FAC.	0.10	
R.A. PLENUMS	NO	
CALC. ADP	NO	

OCCUPANCY

BTU/PERSON, SENS.	255
BTU/PERSON, LAT.	255
LOAD PROFILE NO.	1
SF/PERSON	0.00
MAX. NO. OF PEOPLE	40

LIGHTING

WATTS/SF	9.80
LOAD PROFILE NO.	2
PERCENT TO P.A.	0.

LOAD FACTOR MULTIPLIERS

LIGHTS	0.80
APPLIANCES	0.50
PEOPLE	0.80
PIPE HEAT	1.00

AIR QUANTITY FACTORS

JOB SITE ALTITUDE	0 FT
BAROMETRIC PRESSURE	29.921
AIR DENSITY FACTOR	1.000

VENTILATION

CFM/SF	0.50
CFM/PERSON	10.00
AIR CHANGE/HR	2.60
PCT. FAN CFM	0.00

INFILTRATION

AIR CHANGE/HR	0.00
DIVERSITY FACTOR	0.80

RUN OPTIONS USED 1 2 3 4 5 6 7 8
0 0 1 0 0 1 0 1

AUTOMATED PROCEDURES FOR ENGINEERING CONSULTANTS, INC.

 HVAC CALCULATION, HCC-III(62) CAPACITE-MARTIN AND ASS. SAN JUAN, PR.

 PROJECT - 8495 CENTER FOR ENERGY & ENVIRONMENT RESEARCH 10/12/78 PAGE 12

BUILDING LOADS SUMMARY

	HEAT GAIN - COOLING		HEAT LOSS	
	SENSIBLE	LATENT	HEATING	WINTER GAIN
WINDOW TRANS	20219.		0.	
WINDOW SOLAR	22383.			0.
WALL	66047.		0.	
ROOF/CEILING	7615.		0.	
PARTITION	0.		0.	
FLOOR	0.		0.	
DOOR	0.		0.	
INFILTRATION	0.	0.	0.	
LIGHTS	267076.			267076.
PEOPLE (- 31)	8423.	8423.		8423.
APPLIANCES	87000.	0.		87000.
TOTALS	478765.	8423.	0.	362499.
TOTAL HEAT AT PEAK HOUR	487188.		PLNM HT VENT. 544544.	
SENS. HEAT RATIO	0.99		TOTAL HUMID 554267.	54.5 BTUH/SF
LIGHT HEAT TO P.A.		0.		
SKYLIGHT HEAT TO P.A.		0.	1099811.	HEATING+HUMID
VENTILATION CFM	13000.		182044.	LOSS LESS INT. GAIN
EXHAUST CFM	0.		182044.	LOSS LESS INT.+SOLAR
PUMP HEAT FACTOR		1.00		
BUILDING REFRIGERATION LOAD		1352234.		
TONS OF REFRIGERATION		113.		

REFERENCE VALUES

	AREA	VOLUME	BTUH/SF		BTUH/CF		SF PER		CFM/SF COOL
			COOL	HEAT	COOL	HEAT	TON	MHH	
COOLING	9990.	267732.	135.4		5.1		88.4		2.9
HEATING	0.	0.		0.0		0.0		0.0	
TOTAL BLDG	9990.	267732.	135.4	54.5	5.1	2.0	88.4	18.3	2.9

AUTOMATED PROCEDURES FOR ENGINEERING CONSULTANTS, INC.

HVAC CALCULATION, HCC-III(02) CAPACETE-MARTIN AND ASS. SAN JUAN, PR.

PROJECT - 9495 CENTER FOR ENERGY & ENVIRONMENT RESEARCH 10/17/78 PAGE 1

BUILDING HOURLY COOLING LOADS (*-BLDG. REFG. INCLUDES VENTILATION)

8	9	10	11	12	13	
SENSIBLE						
WIN TRANS	3676.	7352.	11028.	12866.	16542.	19881.
WIN SOLAR	25456.	30323.	30294.	26945.	21006.	17600.
WALL	37542.	37537.	36162.	36162.	37526.	50900.
ROOF/CEILING	5598.	5488.	5379.	5379.	5270.	5270.
FLOOR	0.	0.	0.	0.	0.	0.
DOOR	0.	0.	0.	0.	0.	0.
INFILT	0.	0.	0.	0.	0.	0.
LIGHT TO RM	267076.	267076.	267076.	267076.	227015.	267076.
PEOPLE	8423.	8423.	8423.	8423.	7159.	8423.
APPLIANCE	87000.	87000.	87000.	87000.	73949.	87000.
TOTAL (INCL. PARTITIONS)	434773.	443202.	445364.	443254.	398471.	454552.

LATENT						
INFILT	0.	0.	0.	0.	0.	0.
PEOPLE	8423.	8423.	8423.	8423.	7159.	8423.
APPLIANCE	0.	0.	0.	0.	0.	0.
TOTAL	8423.	8423.	8423.	8423.	7159.	8423.

TOTAL LOAD	443196.	451625.	453787.	451677.	395630.	462975.
BLDG REFG. *	1051655.	1086186.	1114352.	1133461.	1108455.	1280917.
TONS	88	91	93	95	93	103

14	15	16	17	18	19	
SENSIBLE						
WIN TRANS	20219.	20219.	20219.	20219.	18381.	16542.
WIN SOLAR	17554.	19888.	22383.	21453.	10524.	0.
WALL	60169.	64713.	66047.	63861.	61794.	62542.
ROOF/CEILING	5379.	6185.	7615.	9014.	10179.	10939.
FLOOR	0.	0.	0.	0.	0.	0.
DOOR	0.	0.	0.	0.	0.	0.
INFILT	0.	0.	0.	0.	0.	0.
LIGHT TO RM	267076.	267076.	267076.	267076.	0.	0.
PEOPLE	8423.	8423.	8423.	8423.	0.	0.
APPLIANCE	87000.	87000.	87000.	87000.	0.	0.
TOTAL (INCL. PARTITIONS)	455922.	473506.	478765.	477048.	100879.	90024.

LATENT						
INFILT	0.	0.	0.	0.	0.	0.
PEOPLE	8423.	8423.	8423.	8423.	0.	0.
APPLIANCE	0.	0.	0.	0.	0.	0.
TOTAL	8423.	8423.	8423.	8423.	0.	0.

TOTAL LOAD	474245.	481930.	487188.	485471.	100879.	90024.
BLDG REFG. *	1305165.	1343064.	1352234.	1338759.	673111.	633038.
TONS	104	112	113			

$\sum_{10}^8 = 900 \text{ T.R. H}$

AUTOMATED PROCEDURES FOR ENGINEERING CONSULTANTS, INC.

--- HVAC CALCULATION, --CC-III(G?) --CAPACETE--MARTIN AND ASS. SAN JUAN, PR.
 PROJECT - 3495 --CENTED FOR ENERGY & ENVIRONMENT RESEARCH 10/12/78 PAGE 1

WEATHER PROFILES

MONTH	1	2	3	4	5	6	7	8	9	10	11	12
TEMP. (DB)	71.0	73.0	76.0	80.0	82.0	83.0	83.0	83.0	82.0	81.0	80.0	78.0
TEMP. (WB)	67.8	69.7	71.1	72.0	74.5	74.6	74.2	73.6	73.4	72.9	73.2	72.9
HR X 10000	139	140	153	150	167	166	162	157	156	154	159	157

MONTH	1	2	3	4	5	6	7	8	9	10	11	12
TEMP. (DB)	78.0	80.0	83.0	86.0	87.0	88.0	89.0	89.0	87.0	86.0	85.0	85.0
TEMP. (WB)	75.1	76.3	76.0	78.0	79.0	79.6	79.0	78.6	78.9	78.1	78.5	78.4
HR X 10000	182	188	186	190	197	200	194	191	196	191	197	196

GEOGRAPHIC/SOLAR DATA

INWARD FLOW FRACTIONS

LATITUDE	18.44	NI	NIU	MIR
GROUND REFLECTIVITY	0.20	0.33	0.00	0.00
CLEARNESS FACTOR	1.00			
MAX. SOLAR GAIN, BTU/HSF	80.00	DAYLIGHT SVG.	J F M A M J J A S O N D	
DEGS. FROM STD. MERIDIAN	-5.00	IA EFFECT	0 0 0 0 0 0 0 0 0 0 0 0	

DESIGN CONDITIONS

MASTER BUILDING DATA

	WINTER	SUMMER	
INSIDE TEMPERATURE	76.0	76.0	BLDG. ORIENT. 65.0 DEG. CORR. FACT.
RELATIVE HUM	50.0	55.0	WALL HEIGHT 26.80 FEET
HUMIDITY RAT	0.0096	0.0106	HRG. AVERAGE 5
OUTSIDE TEMPERATURE, DB	9.0	88.0	COOLING D.T. 20.0 DEG.
TEMPERATURE, WB	9.0	79.6	HEATING D.T. 50.0 DEG.
MONTH	1	0	HEATING LOAD NO
			COOLING LOAD YES
			OMIT WINT. SUN NO
			CIRC. RATE 0.00 AC/HP, MIN
			COIL R.P. FAC. 0.10
			R.A. PLENUMS NO
			CALC. ADP NO

OCCUPANCY

LIGHTING

BTU/PERSON, SENS.	255.	WATTS/SF	9.80
BTU/PERSON, LAT.	255.	LOAD PROFILE NO.	2
LOAD PROFILE NO.	1	PERCENT TO R.A.	0.
SF/PERSON	0.00		
MAX. NO. OF PEOPLE	40		

LOAD FACTOR MULTIPLIERS

AIR QUANTITY FACTORS

LIGHTS	0.80	JOB SITE ALTITUDE	0 FT
APPLIANCES	0.50	BAROMETRIC PRESSURE	29.921
PEOPLE	0.80	AIR DENSITY FACTOR	1.000
PUMP HEAT	1.00		

VENTILATION

INFILTRATION

CFM/SF	0.50	AIR CHANGE/HR	0.00
CFM/PERSON	10.00	DIVERSITY FACTOR	0.80
AIR CHANGE/HR	2.60		
PCT. FAN CFM	0.00		

1 2 3 4 5 6 7 8
 RUN OPTIONS USED 0 0 1 0 0 1 0 1

AUTOMATED PROCEDURES FOR ENGINEERING CONSULTANTS, INC.

HVAC CALCULATION (ACC-111102) - CAPACETE - MARTIN AND ASS. SAN JUAN, PR.

PROJECT - 8495 CENTER FOR ENERGY & ENVIRONMENT RESEARCH 10/12/78 PAGE 12

BUILDING LOADS SUMMARY

	HEAT GAIN - COOLING		HEAT LOSS	
	SENSIBLE	LATENT	HEATING	WINTER GAIN
WINDOW TRANS	22057.		0.	
WINDOW SOLAR	22561.			0.
WALL	49604.		0.	
ROOF/CEILING	4771.		0.	
PARTITION	0.		0.	
FLOOR	0.		0.	
DOOR	0.		0.	
INFILTRATION	0.	0.	0.	
LIGHTS	267076.			267076.
PEOPLE (31)	8423.	8423.		8423.
APPLIANCES	87000.	0.		87000.
TOTALS	461594.	8423.	0.	362499.
TOTAL HEAT AT PEAK HOUR	470017.		PLNM HT VENT. 506792.	
SENS. HEAT RATIO	0.99		TOTAL HUMID 573144.	50.7 RTUH/SF
LIGHT HEAT TO P.A.		0.		
SKYLIGHT HEAT TO P.A.		0.	1079936.	HEATING+HUMID
VENTILATION CFM	13000.		144292.	LOSS LESS INT. GAIN
EXHAUST CFM	0.		144292.	LOSS LESS INT.+SOLAR
PUMP HEAT FACTOR		1.00		
BUILDING REFRIGERATION LOAD		1332872.		
TONS OF REFRIGERATION		111.		

REFERENCE VALUES

	AREA	VOLUME	RTUH/SF		RTUH/CF		SF PER		CFM/SF COOL
			COOL	HEAT	COOL	HEAT	TON	MBH	
COOLING	9990.	267732.	133.4		5.0		90.0		2.9
HEATING	0.	0.		0.0		0.0		0.0	
TOTAL BLDG	9990.	267732.	133.4	50.7	5.0	1.9	90.0	19.7	2.9

 AUTOMATED PROCEDURES FOR ENGINEERING CONSULTANTS, INC.

 HVAC CALCULATION, HCC-III(02) CAPACITE-MARTIN AND ASS. SAN JUAN, P.R.

PROJECT - 8498 CENTER FOR ENERGY & ENVIRONMENT RESEARCH 10/12/78 PAGE 13

BUILDING HOURLY COOLING LOADS (*-BLDG. REFG. INCLUDES VENTILATION)

HOOR	8	9	10	11	12	13
SENSIBLE						
WIN TRANS	3676.	7352.	12966.	18391.	20219.	22057.
WIN SOLAR	27358.	43452.	43338.	38556.	31284.	22661.
WALL	36095.	35620.	35615.	34239.	34239.	49674.
ROOF/CEILING	5209.	5099.	4960.	4880.	4880.	4771.
FLOOR	0.	0.	0.	0.	0.	0.
DOOR	0.	0.	0.	0.	0.	0.
INFILT	0.	0.	0.	0.	0.	0.
LIGHT TO RM	267076.	267076.	267076.	267076.	227015.	267076.
PEOPLE	8423.	8423.	8423.	8423.	7159.	8423.
APPLIANCE	87000.	87000.	87000.	87000.	73949.	87000.
TOTAL (INCL. PARTITIONS)	445738.	454024.	459300.	458558.	399748.	461594.

LATENT						
INFILT	0.	0.	0.	0.	0.	0.
PEOPLE	8423.	8423.	8423.	8423.	7159.	8423.
APPLIANCE	0.	0.	0.	0.	0.	0.
TOTAL	8423.	8423.	8423.	8423.	7159.	8423.

TOTAL LOAD	454161.	462447.	467732.	466981.	405998.	470017.
BLDG REFG. *	1041251.	1120418.	1170149.	1241056.	1703577.	1332872.
	87	94	97	103	100	111

HOOR	14	15	16	17	18	19
SENSIBLE						
WIN TRANS	22057.	22057.	20219.	18391.	16542.	16542.
WIN SOLAR	15499.	13215.	13793.	12733.	855.	0.
WALL	61258.	65666.	67995.	68124.	66412.	68041.
ROOF/CEILING	4771.	5573.	7157.	8591.	9880.	10847.
FLOOR	0.	0.	0.	0.	0.	0.
DOOR	0.	0.	0.	0.	0.	0.
INFILT	0.	0.	0.	0.	0.	0.
LIGHT TO RM	267076.	267076.	267076.	267076.	0.	0.
PEOPLE	8423.	8423.	8423.	8423.	0.	0.
APPLIANCE	87000.	87000.	87000.	87000.	0.	0.
TOTAL (INCL. PARTITIONS)	466086.	469912.	471665.	470330.	93691.	95431.

LATENT						
INFILT	0.	0.	0.	0.	0.	0.
PEOPLE	8423.	8423.	8423.	8423.	0.	0.
APPLIANCE	0.	0.	0.	0.	0.	0.
TOTAL	8423.	8423.	8423.	8423.	0.	0.

TOTAL LOAD	474509.	477435.	480089.	478754.	93691.	95431.
LDG REFG. *	1307688.	1290813.	1304860.	1244517.	621653.	622030.
	104	107	104			

$\sum \frac{Q}{TA} = 91770. H$

AUTOMATED PROCEDURES FOR ENGINEERING CONSULTANTS, INC.

HVAC CALCULATION, HCC-111(02) CAPACITE-MARTIN AND ASS. SAN JUAN, PR.
 PROJECT - 8495 CENTER FOR ENERGY & ENVIRONMENT RESEARCH 10/12/78 PAGE 1

WEATHER PROFILES

HOURS	9	10	11	12	13	14	15	16	17	18	19	
MONTH 1	71.	73.	76.	80.	82.	83.	83.	83.	82.	81.	80.	DR
	67.8	69.7	71.1	73.0	74.5	74.6	74.2	73.6	73.4	72.9	73.2	WH
	139	140	153	150	167	166	162	157	156	154	159	HR X 1000
MONTH 10	75.	77.	80.	83.	85.	86.	86.	85.	85.	84.	83.	DR
	72.6	73.3	74.2	75.5	77.4	78.4	78.5	77.6	78.0	77.7	77.2	WH
	169	169	169	174	186	193	194	186	192	189	187	HR X 1000

GEOGRAPHIC/SOLAR DATA

LATITUDE	18.44
GROUND REFLECTIVITY	0.20
CLEARNESS FACTOR	1.00
MAX. SOLAR GAIN, BTUH/SF	80.00
DEGS. FROM STD. MERIDIAN	-5.00

INWARD FLOW FRACTIONS

NI	NIU	AIR
0.33	0.00	0.00
DAYLIGHT SVG. J F M A M J J A S O N D		
IN EFFECT 0 0 0 0 0 0 0 0 0 0 0 0		

DESIGN CONDITIONS

	WINTER	SUMMER
INSIDE		
TEMPERATURE	76.0	76.0
RELATIVE HUM	50.0	55.0
HUMIDITY RAT	0.0096	0.0106
OUTSIDE		
TEMPERATURE, DR	0.0	86.0
TEMPERATURE, WR	0.0	78.5
MONTH	1	10

MASTER BUILDING DATA

BLDG. ORIENT.	65.0 DEG. CORR. FACT.
WALL HEIGHT	26.80 FEET
HOHR AVERAGE	5
COOLING D.T.	20.0 DEG.
HEATING D.T.	50.0 DEG.
HEATING LOAD	NO
COOLING LOAD	YES
OMIT WINTP SUN	NO
CIRCN. RATE	0.00 AC/HP, MIN
COIL R.P. FAC.	0.10
R.A. PLENUMS	NO
CALC. ADP	NO

OCCUPANCY

BTU/PERSON, SENS.	255.
BTU/PERSON, LAT.	255.
LOAD PROFILE NO.	1
SE/PERSON	0.00
MAX. NO. OF PEOPLE	40

LIGHTING

WATTS/SF	9.80
LOAD PROFILE NO.	2
PERCENT TO R.A.	0.

LOAD FACTOR MULTIPLIERS

LIGHTS	0.80
APPLIANCES	0.50
PEOPLE	0.80
PUMP HEAT	1.00

AIR QUANTITY FACTORS

JOB SITE ALTITUDE	0 FT
BAROMETRIC PRESSURE	29.921
AIR DENSITY FACTOR	1.000

VENTILATION

CFM/SF	0.50
CFM/PERSON	10.00
AIR CHANGE/HR	2.60
PCT. FAN CFM	0.00

INFILTRATION

AIR CHANGE/HR	0.00
DIVERSITY FACTOR	0.80
1 2 3 4 5 6 7 8	
RUN OPTIONS USED	0 0 1 0 0 1 0 1

AUTOMATED PROCEDURES FOR ENGINEERING CONSULTANTS, INC.

HVAC CALCULATION, HCC-111(02) - CAPACETE-MARTIN AND ASS. SAN JUAN, PR.

PROJECT - R408 CENTER FOR ENERGY & ENVIRONMENT RESEARCH 10/12/78 PAGE 12

BUILDING LOADS SUMMARY

	HEAT GAIN - COOLING		HEAT LOSS	
	SENSIBLE	LATENT	HEATING	WINTER GAIN
WINDOW TRANS	18221.		0.	
WINDOW SOLAR	20472.			0.
WALL	52757.		0.	
ROOF/CEILING	3414.		0.	
PARTITION	0.		0.	
FLOOR	0.		0.	
DOOR	0.		0.	
INFILTRATION	0.	0.	0.	
LIGHTS	267076.			267076.
PEOPLE (31)	8423.	8423.		8423.
APPLIANCES	87000.	0.		87000.
TOTALS	457526.	8423.	0.	362499.
TOTAL HEAT	465949.		PLNW HT	0.
AT PEAK HOUR	14		VENT.	375803.
SENS. HEAT RATIO	1.99		TOTAL HUMID	410696.
LIGHT HEAT TO R.A.		0.		
SKYLIGHT HEAT TO R.A.		0.	786499.	HEATING+HUMID
VENTILATION CFM	13000.		13304.	LOSS-LESS INT. GAIN
EXHAUST CFM	0.		13304.	LOSS LESS INT.+SOLAR
PUMP HEAT FACTOR		1.00		
BUILDING REFRIGERATION LOAD		126399.		
TONS OF REFRIGERATION		105.		

REFERENCE VALUES

	AREA	VOLUME	BTUH/SF		BTUH/CF		SF PER		CFM/SF
			COOL	HEAT	COOL	HEAT	TON	YR	
COOLING	9990.	267732.	126.5		4.7		95.1		2.8
HEATING	0.	0.		0.0		0.0		0.0	
TOTAL BLDG	9990.	267732.	126.5	37.6	4.7	1.4	95.1	26.6	2.8

AUTOMATED PROCEDURES FOR ENGINEERING CONSULTANTS, INC.

HVAC CALCULATION, HCC-BH(02) - CAPACITE - MARTIN AND ASS. SAN JUAN, PR.

PROJECT - 8495 CENTER FOR ENERGY & ENVIRONMENT RESEARCH 10/12/78 PAGE 1

BUILDING HOURLY COOLING LOADS (*-PLDG. REFG. INCLUDES VENTILATION)

HOOR	8	9	10	11	12	13
SENSIBLE						
WIN TRANS	1838.	1838.	7352.	12866.	16542.	18381.
WIN SOLAR	45022.	53133.	53245.	48993.	41738.	31608.
WALL	30720.	29345.	29340.	27965.	27965.	41397.
ROOF/CEILING	3851.	3742.	3632.	3523.	3523.	3414.
FLOOR	0.	0.	0.	0.	0.	0.
DOOR	0.	0.	0.	0.	0.	0.
INFILT	0.	0.	0.	0.	0.	0.
LIGHT TO RM	267076.	267076.	267076.	267076.	227015.	267076.
PEOPLE	8423.	8423.	8423.	8423.	7159.	8423.
APPLIANCE	87000.	87000.	87000.	87000.	73949.	87000.
TOTAL (INCL. PARTITIONS)	441256.	450559.	456071.	455749.	397895.	457291.

LATENT						
INFILT	0.	0.	0.	0.	0.	0.
PEOPLE	8423.	8423.	8423.	8423.	7159.	8423.
APPLIANCE	0.	0.	0.	0.	0.	0.
TOTAL	8423.	8423.	8423.	8423.	7159.	8423.

TOTAL LOAD	449679.	458082.	464494.	464172.	405055.	465714.
PLDG REFG. *	910417.	967955.	1021923.	1098059.	1109474.	1257693.
TONS	77	80	85	92	92	105
HOOR	14	15	16	17	18	19

HOOR	14	15	16	17	18	19
SENSIBLE						
WIN TRANS	18381.	18381.	16542.	16542.	14704.	12866.
WIN SOLAR	20472.	11927.	8273.	5806.	0.	0.
WALL	52757.	57137.	59274.	59215.	61659.	62154.
ROOF/CEILING	3414.	3969.	5431.	6853.	8119.	9050.
FLOOR	0.	0.	0.	0.	0.	0.
DOOR	0.	0.	0.	0.	0.	0.
INFILT	0.	0.	0.	0.	0.	0.
LIGHT TO RM	267076.	267076.	267076.	267076.	0.	0.
PEOPLE	8423.	8423.	8423.	8423.	0.	0.
APPLIANCE	87000.	87000.	87000.	87000.	0.	0.
TOTAL (INCL. PARTITIONS)	457526.	453915.	452022.	450018.	34483.	85071.

LATENT						
INFILT	0.	0.	0.	0.	0.	0.
PEOPLE	8423.	8423.	8423.	8423.	0.	0.
APPLIANCE	0.	0.	0.	0.	0.	0.
TOTAL	8423.	8423.	8423.	8423.	0.	0.

TOTAL LOAD	465049.	462339.	460445.	459341.	84483.	85071.
LDG REFG. *	1263399.	1215163.	1227107.	1209505.	548136.	539846.
TONS	105	101	102			

$\sum_{14}^P = 533172, 117$

AUTOMATED PROCEDURES FOR ENGINEERING CONSULTANTS, INC.

HVAC CALCULATION, HCC-III(02) - CAPACETE-MARTIN AND ASS. SAN JUAN, PP.

PROJECT - 8495 CENTER FOR ENERGY & ENVIRONMENT RESEARCH 10/12/78 PAGE

WEATHER PROFILES

HOURS	8	9	10	11	12	13	14	15	16	17	18	19	
MONTH 1	71.	73.	76.	80.	82.	83.	83.	83.	83.	82.	81.	80.	DR
	67.8	69.7	71.1	73.0	74.5	74.6	74.2	73.6	73.4	72.9	73.2	72.8	WR
	139	149	153	159	167	166	162	157	156	154	159	157	HR X 1000
MONTH 11	74.	76.	79.	82.	84.	85.	85.	85.	85.	84.	83.	82.	DR
	70.6	71.5	72.4	74.3	75.6	76.3	76.3	75.6	75.3	75.3	75.1	75.2	WR
	154	156	157	166	172	176	176	170	167	170	170	173	HR X 1000

GEOGRAPHIC/SOLAR DATA

LATITUDE	18.44
GROUND REFLECTIVITY	0.20
CLEARNESS FACTOR	1.00
MAX. SOLAR GAIN, BTU/H/SF	80.00
DEGS. FROM STD. MERIDIAN	-5.00

INWARD FLOW FRACTIONS

MI	NIU	NIR
0.33	0.00	0.00
DAYLIGHT SVGS. J F M A M J J A S O N D		
IN EFFECT 0 0 0 0 0 0 0 0 0 0 0 0		

DESIGN CONDITIONS

	WINTER	SUMMER
INSIDE TEMPERATURE	74.0	76.0
RELATIVE HUM	50.0	55.0
HUMIDITY RAT	0.0096	0.0106
OUTSIDE TEMPERATURE, DR	0.0	95.0
TEMPERATURE, WR	0.0	76.3
MONTH	1	11

MASTER BUILDING DATA

BLDG. ORIENT.	65.0 DEG. CORR. FACT.
WALL HEIGHT	26.80 FEET
HOHR AVERAGE	5
COOLING D.T.	20.0 DEG.
HEATING D.T.	50.0 DEG.
HEATING LOAD	NO
COOLING LOAD	YES
OMIT WINT. SUN	NO
CIRCN. RATE	0.00 AC/HR, MIN
COIL R.P. FAC.	0.10
R.A. PLENUMS	NO
GALC. ADP	NO

OCCUPANCY

BTU/PERSON, SENS.	255.
BTU/PERSON, LAT.	255.
LOAD PROFILE NO.	1
SE/PERSON	0.00
MAX. NO. OF PEOPLE	40

LIGHTING

WATTS/SF	9.80
LOAD PROFILE NO.	2
PERCENT TO R.A.	0.

LOAD FACTOR MULTIPLIERS

LIGHTS	0.80
APPLIANCES	0.50
PEOPLE	0.80
PUMP HEAT	1.00

AIR QUANTITY FACTORS

JOB SITE ALTITUDE	0 FT
BAROMETRIC PRESSURE	29.921
AIR DENSITY FACTOR	1.000

VENTILATION

CFM/SF	0.50
CFM/PERSON	10.00
AIR CHANGE/HR	2.60
PCT. FAN CFM	0.00

INFILTRATION

AIR CHANGE/HR	0.00
DIVERSITY FACTOR	0.80

PUM. OPTIONS USED 1 2 3 4 5 6 7 8
0 0 1 0 0 1 0 1

AUTOMATED PROCEDURES FOR ENGINEERING CONSULTANTS, INC.

HWAC CALCULATION, HCC-111(02) CAPACITE-MARTIN AND ASS. SAN JUAN, PR.
 PROJECT - 8498 CENTER FOR ENERGY & ENVIRONMENT RESEARCH 10/12/78 PAGE 11

BUILDING LOADS SUMMARY

	HEAT GAIN - COOLING		HEAT LOSS	
	SENSIBLE	LATENT	HEATING	WINTER GAIN
WINDOW TRANS	14542.		0.	
WINDOW SOLAR	29362.			0.
WALL	46906.		0.	
ROOF/CEILING	2165.		0.	
PARTITION	0.		0.	
FLOOR	0.		0.	
DOOR	0.		0.	
INFILTRATION	0.	0.	0.	
LIGHTS	267076.			267076.
PEOPLE (31)	8423.	8423.		8423.
APPLIANCES	97000.	0.		97000.
TOTALS	457477.	8423.	0.	362499.
TOTAL HEAT	465900.		PLNM HT 0.	
AT PEAK HOUR	14		VENT. 273416.	
SENS. HEAT RATIO	0.98		TOTAL 273416.	27.4 BTUH/SF
			HUMID 314600.	
LIGHT HEAT TO R.A.		0.		
SKYLIGHT HEAT TO R.A.		0.	589016.	HEATING+HUMID
VENTILATION CFM	12000.		-89093.	LOSS LESS INT. GAIN
EXHAUST CFM	0.		-89093.	LOSS LESS INT.+SOLAR
PUMP HEAT FACTOR		1.00		
BUILDING REFRIGERATION LOAD		1144506.		
TONS OF REFRIGERATION		95.		

REFERENCE VALUES

	AREA	VOLUME	BTUH/SF		BTUH/CF		SF PER TOT. YRH	CFM/SF COOL
			COOL	HEAT	COOL	HEAT		
COOLING	9990.	267732.	114.6		4.3		105.2	2.8
HEATING	0.	0.		0.0		0.0	0.0	
TOTAL PLOG	9990.	267732.	114.6	27.4	4.3	1.0	105.2	36.5

AUTOMATED PROCEDURES FOR ENGINEERING CONSULTANTS, INC.

HVAC CALCULATION, HCC-III(02) - CAPACITE-MARTIN AND ASS. SAN JUAN, PR.

PROJECT - R495 CENTER FOR ENERGY & ENVIRONMENT RESEARCH 10/12/78 PAGE 1

BUILDING HOURLY COOLING LOADS (*-PLUG. REFG. INCLUDES VENTILATION)

HOURLY	8	9	10	11	12	13
SENSIBLE						
WIN TRANS	2476.	0.	5514.	11028.	14704.	16542.
WIN SOLAR	49143.	58880.	60239.	57142.	50811.	41218.
WALL	24210.	24835.	24830.	23455.	23455.	31543.
ROOF/CEILING	2602.	2492.	2383.	2274.	2274.	2155.
FLOOR	0.	0.	0.	0.	0.	0.
DOOR	0.	0.	0.	0.	0.	0.
INFILT	0.	0.	0.	0.	0.	0.
LIGHT TO RM	267076.	267076.	267076.	267076.	227015.	267076.
PEOPLE	8423.	8423.	8423.	8423.	7159.	8423.
APPLIANCE	87000.	87000.	87000.	87000.	73949.	87000.
TOTAL (INCL. PARTITIONS)	436779.	448708.	455467.	456400.	399371.	453970.
LATENT						
INFILT	0.	0.	0.	0.	0.	0.
PEOPLE	8423.	8423.	8423.	8423.	7159.	8423.
APPLIANCE	0.	0.	0.	0.	0.	0.
TOTAL	8423.	8423.	8423.	8423.	7159.	8423.
TOTAL LOAD	445202.	457132.	463890.	464923.	406530.	462403.
PLUG REFG. *	225514.	275712.	2940516.	1039458.	1024796.	1130425.
TONS	69	73	78	87	85	95
HOURLY	14	15	16	17	18	19
SENSIBLE						
WIN TRANS	16542.	16542.	16542.	14704.	12866.	11028.
WIN SOLAR	29352.	17365.	8204.	2662.	0.	0.
WALL	46906.	52186.	54730.	55364.	59255.	60772.
ROOF/CEILING	2155.	2402.	3787.	5182.	6432.	7358.
FLOOR	0.	0.	0.	0.	0.	0.
DOOR	0.	0.	0.	0.	0.	0.
INFILT	0.	0.	0.	0.	0.	0.
LIGHT TO RM	267076.	267076.	267076.	267076.	0.	0.
PEOPLE	8423.	8423.	8423.	8423.	0.	0.
APPLIANCE	87000.	87000.	87000.	87000.	0.	0.
TOTAL (INCL. PARTITIONS)	457477.	450097.	445764.	440413.	78555.	79159.
LATENT						
INFILT	0.	0.	0.	0.	0.	0.
PEOPLE	8423.	8423.	8423.	8423.	0.	0.
APPLIANCE	0.	0.	0.	0.	0.	0.
TOTAL	8423.	8423.	8423.	8423.	0.	0.
TOTAL LOAD	465900.	450420.	454187.	448936.	78555.	79159.
PLUG REFG. *	1144536.	1102752.	1070108.	1071060.	462767.	450091.
TONS	95	98	90			

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AUTOMATED PROCEDURES FOR ENGINEERING CONSULTANTS, INC.

HVAC CALCULATION, HCC-III(02) CAPACITE-MARTIN AND ASS. SAN JUAN, PR.
 PROJECT - 8495 CENTER FOR ENERGY & ENVIRONMENT RESEARCH 10/12/78 PAGE

WEATHER PROFILES

HOURS	8	9	10	11	12	13	14	15	16	17	18	19	
MONTH 1	71.	73.	76.	80.	82.	83.	83.	83.	83.	82.	81.	80.	DR
	67.8	69.7	71.1	73.0	74.5	74.6	74.2	73.6	73.4	72.9	73.2	72.9	WR
	139	149	153	159	167	166	162	157	156	154	159	157	HR X 1000
MONTH 12	75.	77.	78.	79.	81.	81.	81.	81.	81.	80.	79.	78.	DR
	70.8	71.9	72.0	71.9	72.1	72.3	72.2	72.1	72.1	71.9	70.9	70.7	WR
	153	157	156	152	149	151	150	149	149	150	144	145	HR X 1000

GEOGRAPHIC/SOLAR DATA

LATITUDE	18.44
GROUND REFLECTIVITY	0.20
CLEARNESS FACTOR	1.00
MAX. SOLAR GAIN, BTUH/SF	80.00
DEGS. FROM STD. MERIDIAN	-5.00

INWARD FLOW FRACTIONS

NI	NIU	NIR
0.33	0.00	0.00
DAYLIGHT SVGS. J F V A M J J A S O N D		
IN EFFECT 0 0 0 0 0 0 0 0 0 0 0 0		

DESIGN CONDITIONS

	WINTER	SUMMER
INSIDE		
TEMPERATURE	76.0	76.0
RELATIVE HUM	50.0	55.0
HUMIDITY RAT	0.0096	0.0106
OUTSIDE		
TEMPERATURE, DR	0.0	81.0
TEMPERATURE, WR	0.0	72.3
MONTH	1	12

MASTER BUILDING DATA

BLDG. ORIENT.	65.0 DEG.	CORR. FACT.
WALL HEIGHT	26.00 FEET	
HOUR AVERAGE	5	
COOLING D.T.	20.0 DEG.	
HEATING D.T.	50.0 DEG.	
HEATING LOAD	NO	
COOLING LOAD	YES	
OMIT WINT. SUN	NO	
CIRCN. RATE	0.00 AC/HR, MIN	
COIL R.P. FAC.	0.10	
R.A. PLENUMS	NO	
CALC. APP	NO	

OCCUPANCY

RTU/PERSON, SENS.	255.
RTU/PERSON, LAT.	255.
LOAD PROFILE NO.	1
SF/PERSON	0.00
MAX. NO. OF PEOPLE	40

LIGHTING

WATTS/SF	9.80
LOAD PROFILE NO.	2
PERCENT TO R.A.	0.

LOAD FACTOR MULTIPLIERS

LIGHTS	0.90
APPLIANCES	0.50
PEOPLE	0.80
PUMP HEAT	1.00

AIR QUANTITY FACTORS

JOB SITE ALTITUDE	0 FT
BAROMETRIC PRESSURE	29.921
AIR DENSITY FACTOR	1.000

VENTILATION

CFM/SF	0.50
CFM/PERSON	10.00
AIR CHANGE/HR	2.60
PCT. FAN CFM	0.00

INFILTRATION

AIR CHANGE/HR	0.00
DIVERSITY FACTOR	0.80

1 2 3 4 5 6 7 8
 RUN OPTIONS USED 0 0 1 0 0 1 0 1

AUTOMATED PROCEDURES FOR ENGINEERING CONSULTANTS, INC.

HVAC CALCULATION, HCC-III(02) - CAPACITE-MARTIN AND ASS. SAN JUAN, PR.

PROJECT - 8495 CENTER FOR ENERGY & ENVIRONMENT RESEARCH 10/12/78 PAGE 1

BUILDING LOADS SUMMARY

	HEAT GAIN - COOLING		HEAT LOSS	
	SENSIBLE	LATENT	HEATING	WINTER GAIN
WINDOW TRANS	9190.		0.	
WINDOW SOLAR	35360.			0.
WALL	36032.		0.	
ROOF/CEILING	376.		0.	
PARTITION	0.		0.	
FLOOR	0.		0.	
DOOR	0.		0.	
INFILTRATION	0.	0.	0.	
LIGHTS	267076.			267076.
PEOPLE (31)	8423.	8423.		8423.
APPLIANCES	87000.	0.		87000.
TOTALS	443459.	8423.	0.	362499.
TOTAL HEAT AT PEAK HOUR	451982.		PLNM HT VENT. 281424.	
SENS. HEAT RATIO	0.98		TOTAL HUMID 335191.	28.2 BTUH/SF
LIGHT HEAT TO P.A.	0.			
SKYLIGHT HEAT TO P.A.	0.		616615.	HEATING+HUMID
VENTILATION CFM	13000.		-81075.	LOSS LESS INT. GAIN
EXHAUST CFM	0.		-81075.	LOSS LESS INT.+SOLAR
DUMP HEAT FACTOR		1.00		
BUILDING REFRIGERATION LOAD		921072.		
TONS OF REFRIGERATION		77.		

REFERENCE VALUES

	AREA	VOLUME	BTUH/SF		BTUH/CF		SF PER		CFM/SF
			COOL	HEAT	COOL	HEAT	TON	YR	
COOLING	9990.	267732.	92.2		3.4		129.7		2.7
HEATING	0.	0.		0.0		0.0		0.0	
TOTAL BLDG	9990.	267732.	92.2	28.2	3.4	1.1	129.7	35.5	2.7

AUTOMATED PROCEDURES FOR ENGINEERING CONSULTANTS, INC.

HVAC CALCULATION, HCC-III(02) CAPACITY - MARTIN AND ASS. SAN JUAN, PR.

PROJECT - 8485 CENTER FOR ENERGY & ENVIRONMENT RESEARCH 10/12/78 PAGE 12

BUILDING HOURLY COOLING LOADS (*-BLDG. REFG. INCLUDES VENTILATION)

MOHP	8	9	10	11	12	13
SENSIBLE						
WIN TRANS	1430.	1039.	3676.	5514.	9190.	9190.
WIN SOLAR	45478.	59377.	62605.	60651.	55337.	46672.
WALL	10783.	9408.	10778.	10773.	12148.	15240.
ROOF/CEILING	376.	267.	267.	158.	267.	267.
FLOOR	0.	0.	0.	0.	0.	0.
DOOR	0.	0.	0.	0.	0.	0.
INFILT	0.	0.	0.	0.	0.	0.
LIGHT TO RM	267076.	267076.	267076.	267076.	227015.	267076.
PEOPLE	8423.	8423.	8423.	8423.	7159.	8423.
APPLIANCE	87000.	87000.	87000.	87000.	73949.	87000.
TOTAL (INCL. PARTITIONS)	417299.	433391.	430827.	439596.	385068.	433870.

LATENT						
INFILT	0.	0.	0.	0.	0.	0.
PEOPLE	8423.	8423.	8423.	8423.	7159.	8423.
APPLIANCE	0.	0.	0.	0.	0.	0.
TOTAL	8423.	8423.	8423.	8423.	7159.	8423.

TOTAL LOAD	425722.	441914.	448250.	449019.	392223.	442203.
BLDG REFG. *	805219.	877291.	899149.	893436.	834713.	913226.
TONS	67	73	75	74	70	76

MOHP	14	15	16	17	18	19
SENSIBLE						
WIN TRANS	9190.	9190.	9190.	7352.	5514.	3676.
WIN SOLAR	35360.	22844.	11502.	3525.	0.	0.
WALL	36032.	43125.	43744.	41754.	45740.	46099.
ROOF/CEILING	376.	599.	1798.	3210.	4286.	5053.
FLOOR	0.	0.	0.	0.	0.	0.
DOOR	0.	0.	0.	0.	0.	0.
INFILT	0.	0.	0.	0.	0.	0.
LIGHT TO RM	267076.	267076.	267076.	267076.	0.	0.
PEOPLE	8423.	8423.	8423.	8423.	0.	0.
APPLIANCE	87000.	87000.	87000.	87000.	0.	0.
TOTAL (INCL. PARTITIONS)	443459.	439259.	428926.	419342.	55540.	54829.

LATENT						
INFILT	0.	0.	0.	0.	0.	0.
PEOPLE	8423.	8423.	8423.	8423.	0.	0.
APPLIANCE	0.	0.	0.	0.	0.	0.
TOTAL	8423.	8423.	8423.	8423.	0.	0.

TOTAL LOAD	461982.	446692.	437240.	426765.	55540.	54829.
BLDG REFG. *	921072.	908476.	905706.	869975.	264487.	241657.
TONS	77	75	74			

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ATTACHMENT #2

C.E.E.R. NEW WING

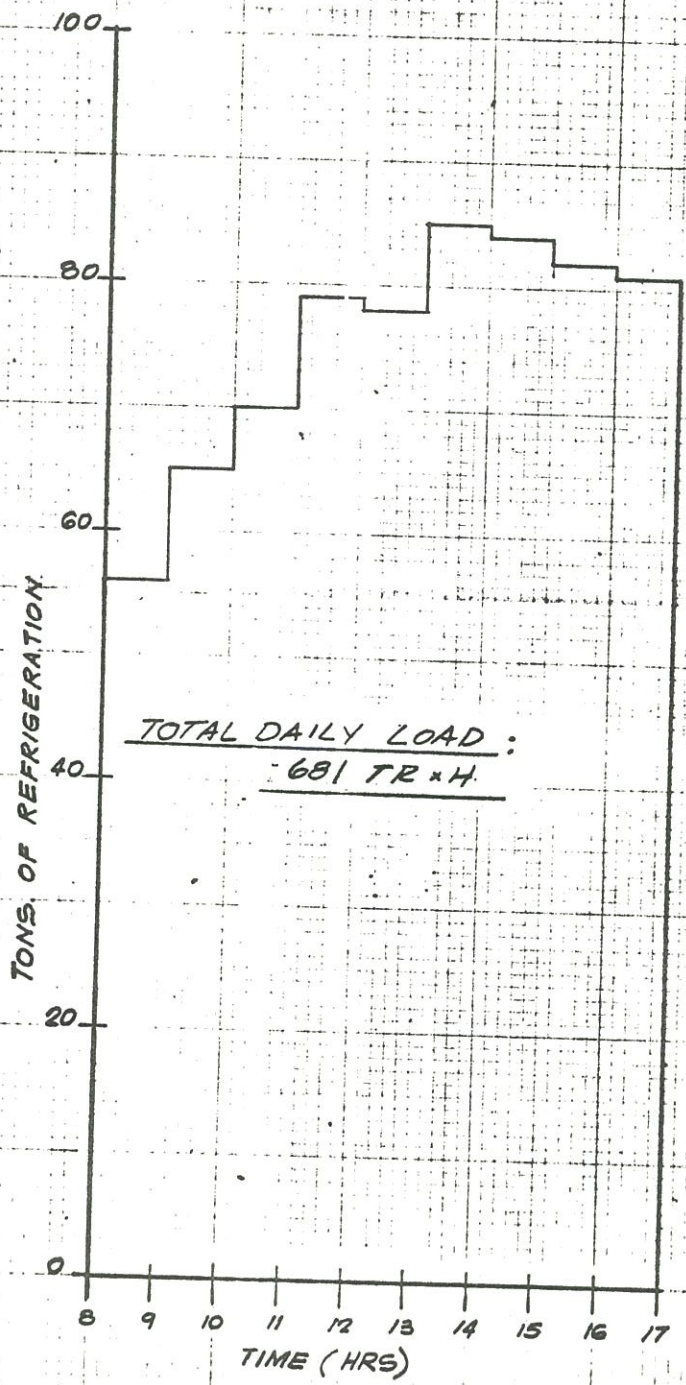
COOLING LOAD PROFILES

C.E.E.R. - New Wing
Cooling Load Profiles

Summary

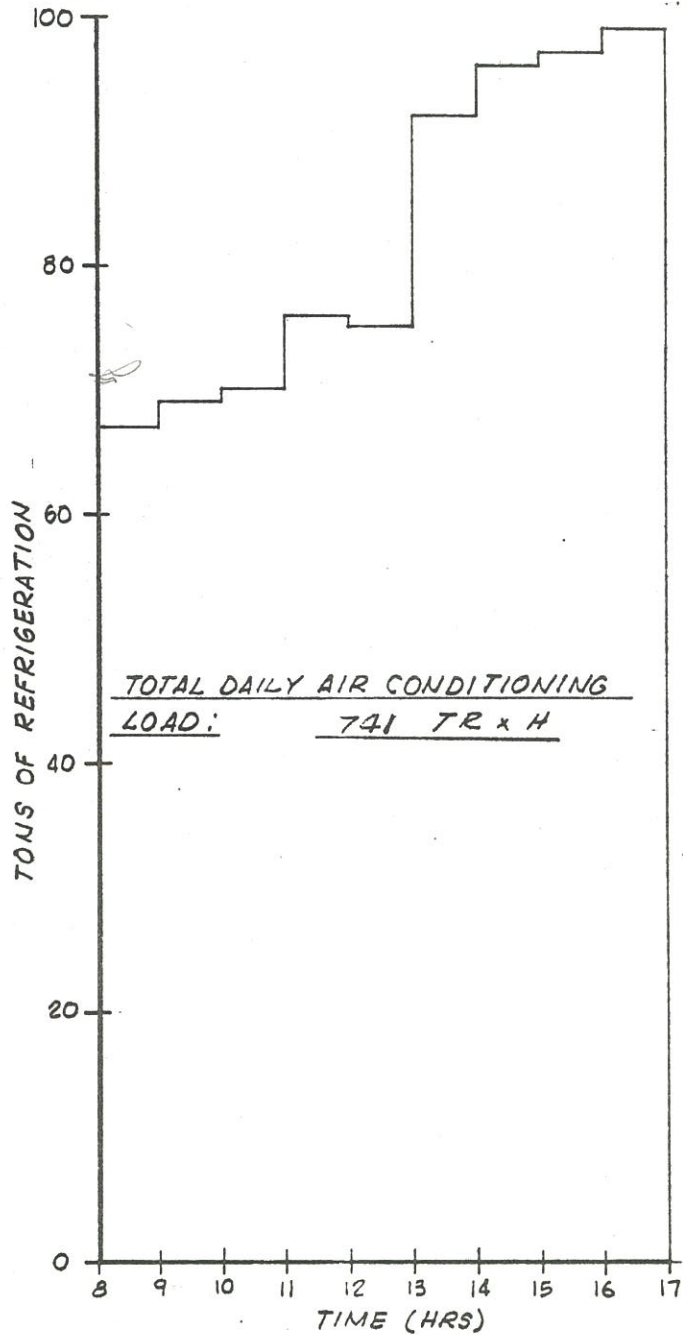
	<u>Sheet</u>
C.E.E.R. New Wing	
Building hourly Cooling Load	
Profile for January (1)	
(Typical Day)	1 of 4
Same for May (5)	2 of 4
Same for September (9)	3 of 4
C.E.E.R. New Wing Year Cooling	
Load Profile at 4:00 p.m. (hour 16)	4 of 4

C.E.E.R. NEW WING
BUILDING HOURLY COOLING LOAD
PROFILE FOR JANUARY (1)
(TYPICAL DAY)



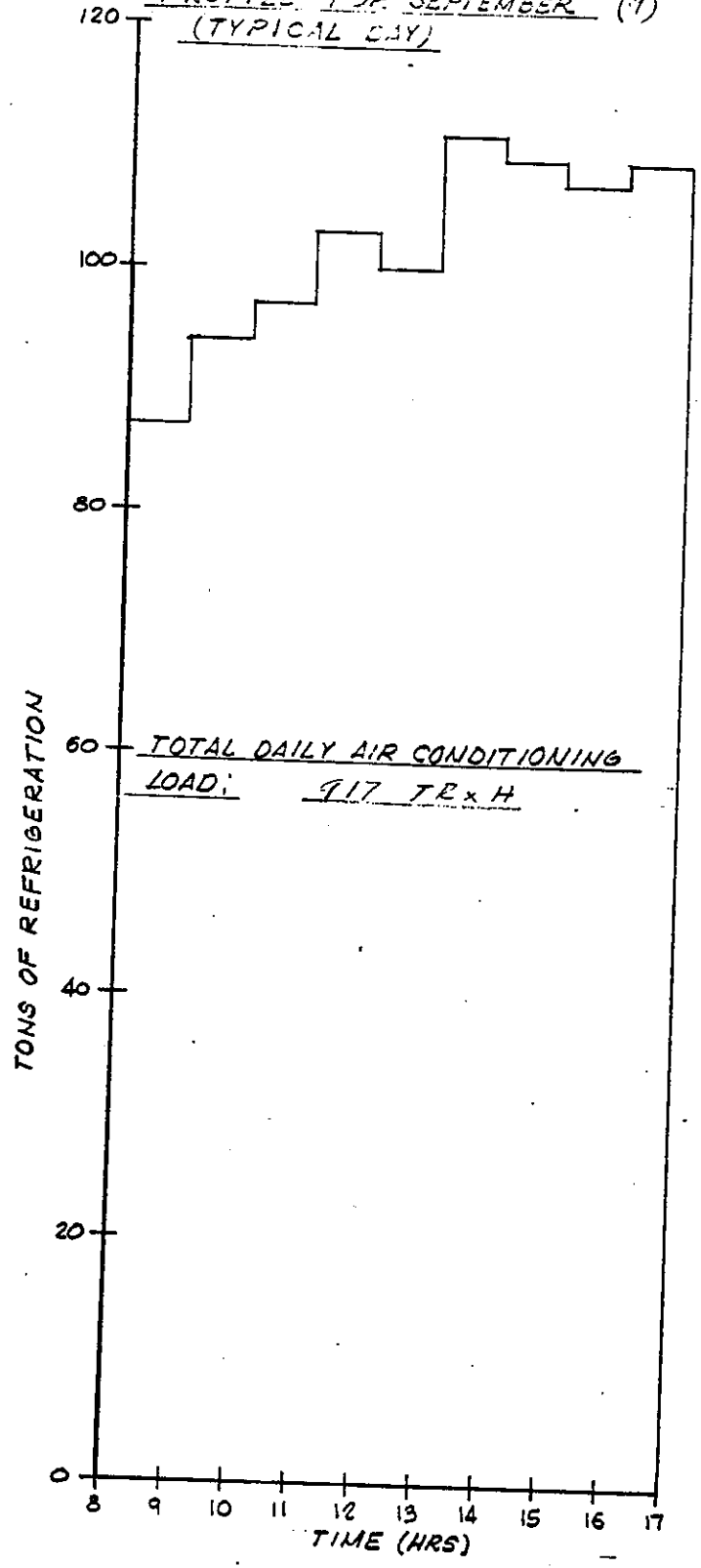
BY R. M. DATE 1/21/78 SUBJECT _____
 CHD. BY P.M. DATE 1/21/78 SHEET NO. 1 OF 4
 JOB NO. 8815

C.E.E.R. NEW WING BUILDING
HOURLY COOLING LOAD
PROFILE FOR MAY (5)
(TYPICAL DAY)



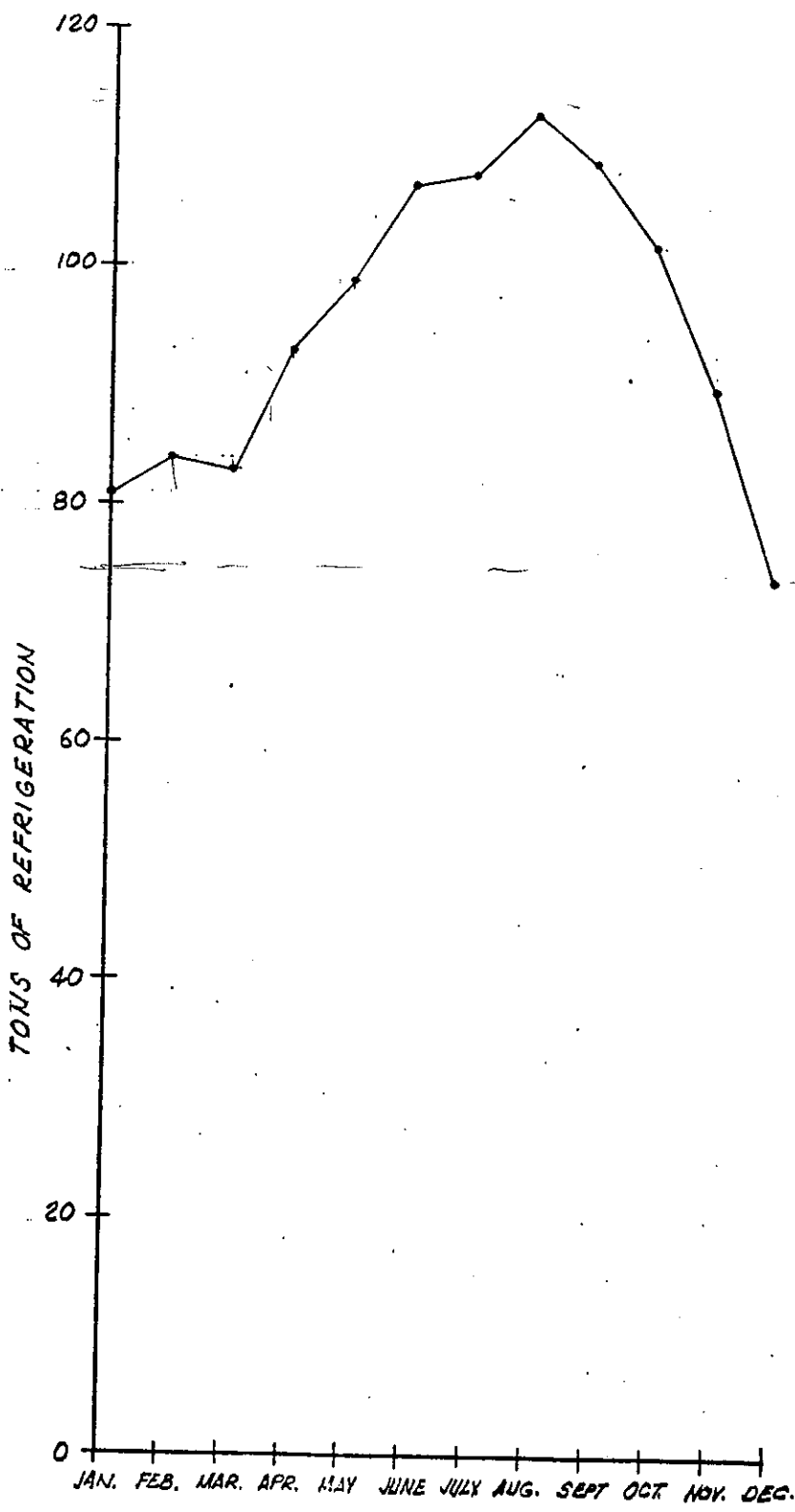
BY R. M. DATE 11/29/78
 CHKD. BY F.M. DATE 11/29/78
 SUBJECT
 SHEET NO. 2 OF 4
 JOB NO. 8995

C.E.E.R. NEW WINS BUILDING
HOURLY COOLING LOAD
PROFILE FOR SEPTEMBER (1)
(TYPICAL DAY)



BY: R.M. DATE: _____
 CHD. BY: F.M. DATE: 11/24/77
 SUBJECT: _____
 SHEET NO. 3 OF 4
 JOB NO. 8495

C.E.E.R. NEW WING BUILDING
YEAR COOLING LOAD PROFILE
AT 4:00 P.M. (HOUR 16)



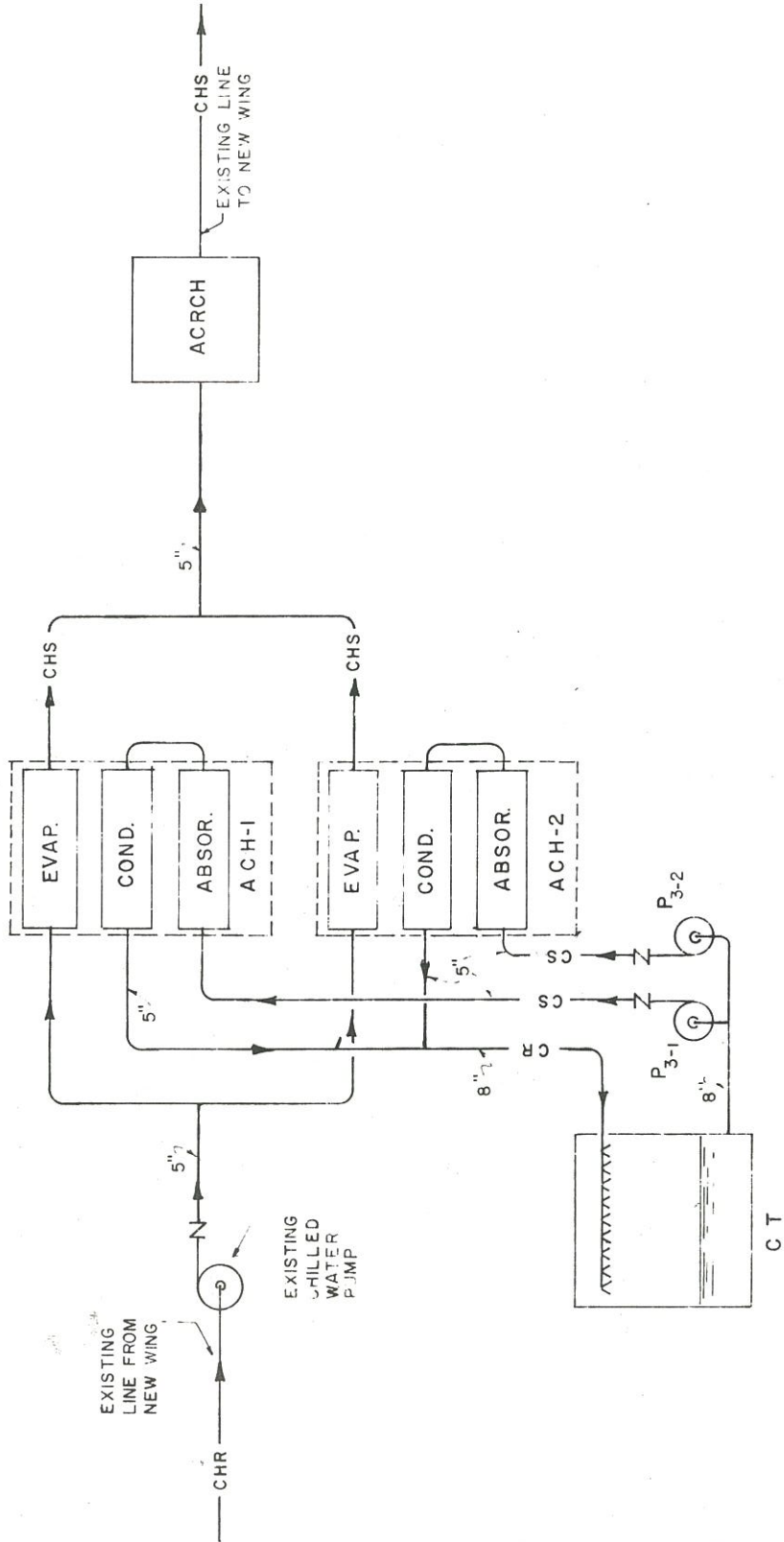
BY R.M. DATE 11/24/88
 CHKD. BY F.M.L. DATE 11/24/88
 SUBJECT _____
 SHEET NO. 4 OF 4
 JOB NO. 5475

ATTACHMENT #3

SCHEMATIC OF THE SOLAR ARRAY
PIPING SYSTEM IN CONJUNCTION
WITH THE ABSORPTION CHILLERS

JOB NO. **8495**
SHEET NO.

SCHEMATIC OF THE CHILLED WATER
AND CONDENSING WATER PIPING SYSTEM



CONCENTRATING PHOTOVOLTAICS FOR THE TROPICS
CENTER FOR ENERGY AND ENVIRONMENT RESEARCH

NONE
DATE 10/13/78

2-5-79
F.M.L.
REVISION

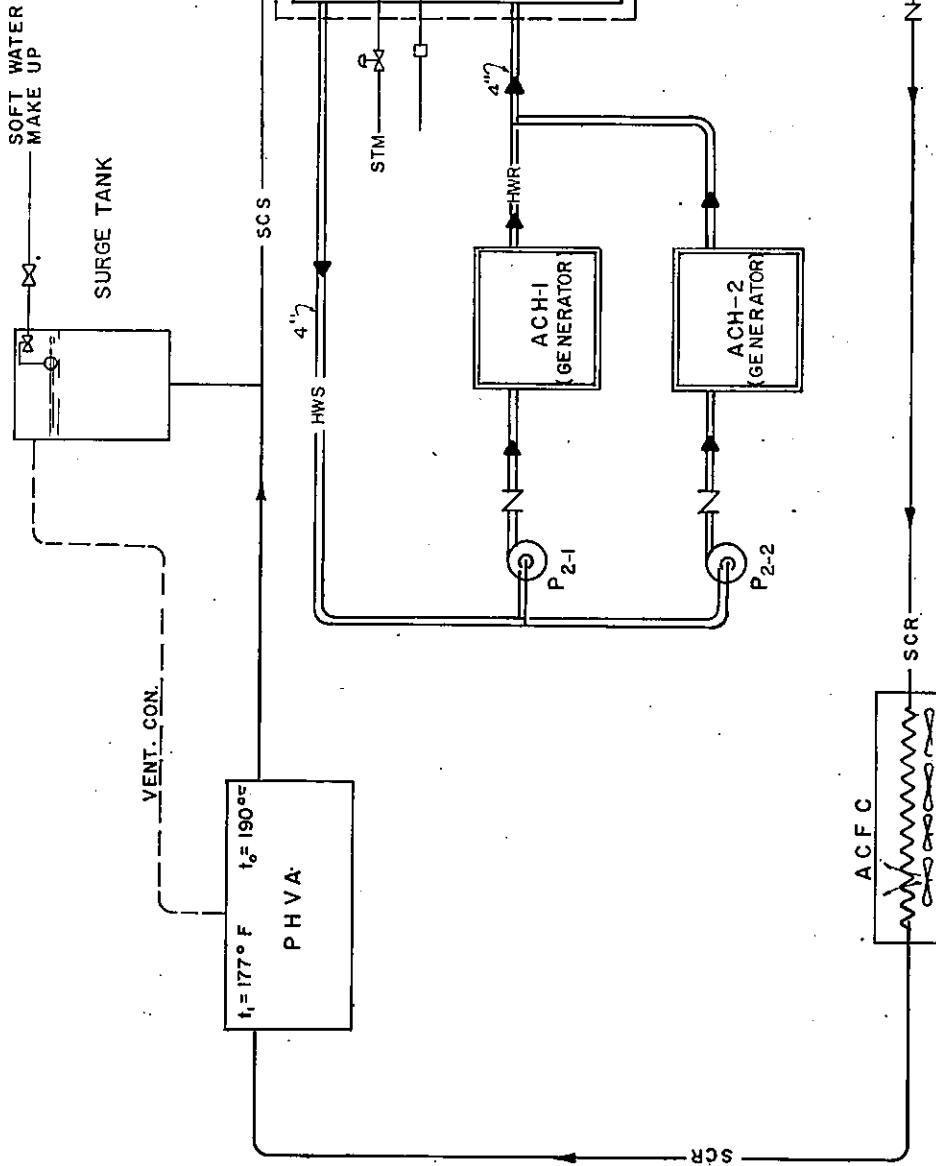
CAPACETE - MARTIN & ASSOCIATES
ARCHITECTS - ENGINEERS
505, P.D. ROOSEVELT AVE., SAN JUAN, P.R.

ATTACHMENT #4

SCHEMATIC OF THE CHILLED WATER
AND CONDENSING WATER PIPING
SYSTEM

JOB NO. 8495
SHEET NO.

**SCHMATIC OF THE SOLAR ARRAY
PIPING SYSTEM IN CONJUNCTION WITH
THE ABSORPTION CHILLERS**



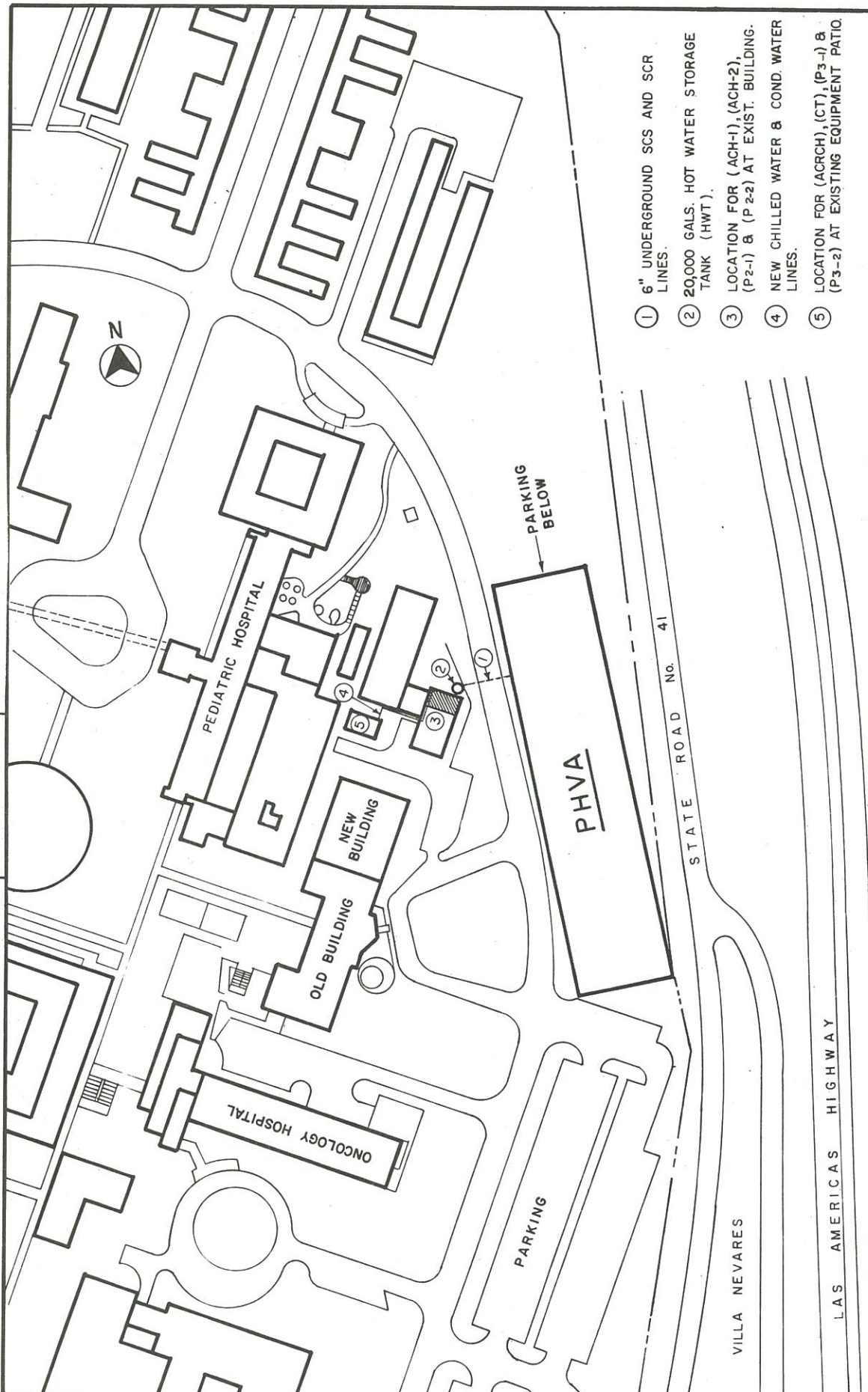
CAPACETE - MARTIN & ASSOCIATES ARCHITECTS - ENGINEERS 1509 F.D. ROOSEVELT AVE., SAN JUAN, P.R.	10-17-78	2-5-79						SCALE	NONE	CONCENTRATING PHOTOVOLTAICS FOR THE TROPICS
	F.M.L.	F.M.L.						DATE	10/13/78	CENTER FOR ENERGY AND ENVIRONMENT RESEARCH
	REVISIONS									

ATTACHMENT #5

GENERAL PLAN

JOB NO. 8495

SHEET NO.



- ① 6" UNDERGROUND SCS AND SCR LINES.
- ② 20,000 GALS. HOT WATER STORAGE TANK (HWT).
- ③ LOCATION FOR (ACH-1), (ACH-2), (P2-1) & (P2-2) AT EXIST. BUILDING.
- ④ NEW CHILLED WATER & COND. WATER LINES.
- ⑤ LOCATION FOR (ACRCH), (CT), (P3-1) & (P3-2) AT EXISTING EQUIPMENT PATIO.

**CONCENTRATING PHOTOVOLTAICS FOR THE TROPICS
CENTER FOR ENERGY AND ENVIRONMENT RESEARCH**

SCALE 1" = 100'
DATE 10/13/78

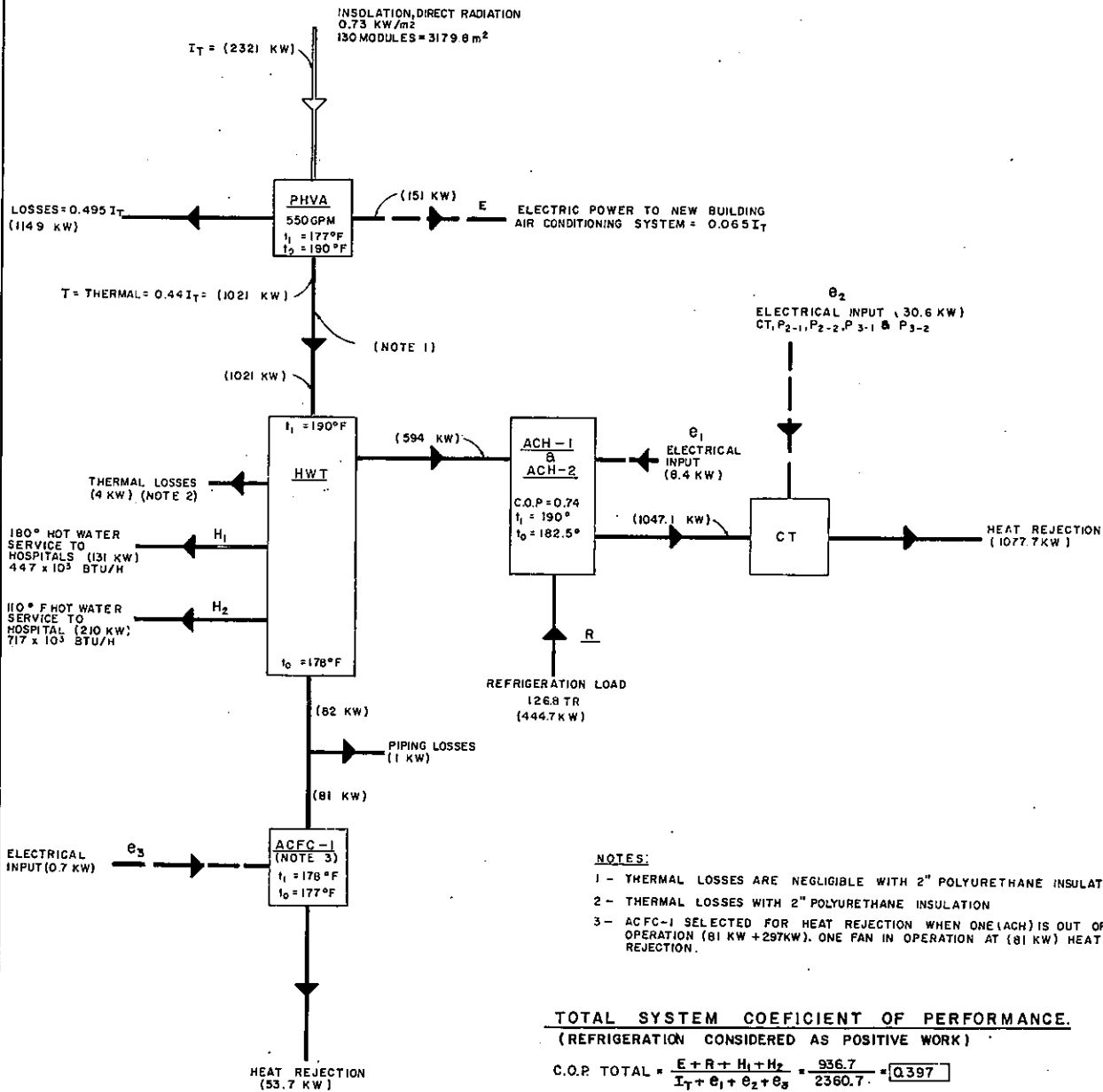
REVISIONS	

10-17-78
F.M.L.
CAPACETE - MARTIN & ASSOCIATES
ARCHITECTS - ENGINEERS
1509 F.D. ROOSEVELT AVE., SAN JUAN, P.R.

ATTACHMENT #6

POWER FLOW DIAGRAM DURING
THE PEAK HOUR INSOLATION

**CO-GENERATION
POWER FLOW DIAGRAM DURING THE PEAK HOUR
INSOLATION INCLUDING SOLAR COOLING**



- NOTES:**
- 1 - THERMAL LOSSES ARE NEGLIGIBLE WITH 2" POLYURETHANE INSULATION.
 - 2 - THERMAL LOSSES WITH 2" POLYURETHANE INSULATION
 - 3 - ACFC-1 SELECTED FOR HEAT REJECTION WHEN ONE (ACH) IS OUT OF OPERATION ($81 \text{ kW} + 297 \text{ kW}$). ONE FAN IN OPERATION AT $(81) \text{ kW}$ HEAT REJECTION.

**TOTAL SYSTEM COEFFICIENT OF PERFORMANCE.
(REFRIGERATION CONSIDERED AS POSITIVE WORK)**

$$\text{C.O.P. TOTAL} = \frac{E + R + H_1 + H_2}{I_T + \theta_1 + \theta_2 + \theta_3} = \frac{936.7}{2360.7} = \boxed{0.397}$$

$$\text{C.O.P. THERMAL} = \frac{R + H_1 + H_2}{T + \theta_1 + \theta_2 + \theta_3} = \frac{787.7}{1060.7} = \boxed{0.743}$$

ATTACHMENT #7

GENERAL INFORMATION FOR
ECONOMIC ANALYSIS

GENERAL INFORMATION FOR ECONOMIC ANALYSES

RECURRING COST

Expenses for electric energy, fuel (or steam purchased from a central plant), material consumed in operation, maintenance services and other items incurred in an annual basis.

DISCOUNT RATE-INTEREST RATE

That rate which is used to transform future investment costs into a value of equivalent worth (see "Present Value"). It enables one to compare investments which have dissimilar cost streams.

DISCOUNTING

The discounted cost of an investment represent the return that would be earned if the money obtained through taxation and spent by the Government were retained by the private sector and allowed to earn a return on its investment opportunities.

PRESENT VALUE

Each year's expected yearly cost multiplied by its discount factor and then summed over all years of the planning period.

DISCOUNT FACTOR-PRESENT VALUE FACTOR

Present value of one (1) dollar. Factors are based on continuous compounding of interest at stated effective rate per annum, assuming uniform cash flow throughout stated one (1) year periods. These factors are equivalent to an arithmetic average of beginning and end of the year compound amount factors found in standard present value tables.

GENERAL INFORMATION FOR ECONOMIC ANALYSIS (cont'd.)TERMINAL VALUE

The expected value of assets at the end of their economic life.

UNIFORM ANNUAL COST

The average cost per year for those years in which benefits accrue. It is obtained by dividing the total present value cost by the sum of the present value factors of the years in which benefits accrue.